



# **Engineering Assessment Report**

Carmanhall Road SHD 2022

August 2022

**Waterman Moylan Consulting Engineers Limited** 

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## Quality Assurance - Approval Status

This document has been prepared and checked in accordance with Waterman Group's IMS (BS EN ISO 9001: 2015, BS EN ISO 14001: 2015)

Issue Date Prepared by Checked by Approved by
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Comments

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## 1. Introduction

Waterman Moylan have been appointed on behalf of Atlas GP Limited. To prepare this Engineering Assessment Report to accompany a planning application to An Bord Pleanala (ABP) for a Strategic Housing Development development on a brownfield site at the junction of Carmanhall Road and Blackthorn Road, Sandyford, Dublin 18. It is also proposed to provide 1 No. Creche along with resident support facilities/resident services and amenities as part of the proposed development.

This report describes the criteria used to design the storm water discharge, disposal of foul water, water supply and vehicular access to the developed site.

#### 2. **Site Description**

#### 2.1 **Site Location**

The subject site is located at Sandyford in south County Dublin. The site which has an area of 0.99ha is located at the junction of Carmanhall Road and Blackthorn Road, Sandyford, Dublin 18. It was formerly occupied by Avid Technology.

At the time of writing in June 2022, the site was vacant.

The adjoining site to the west at the junction of Carmanhall Road and Ravens Rock Road was formerly occupied by Tack Packaging. It extends to 0.57 ha.

Refer to Figure 2-1 for the location of the proposed development.

Figure 2-1 Site Location Map (Google Images)



#### 2.2 **Site Description**

The site comprises the former Avid Technology site the junction of Carmanhall Road and Blackthorn Road. The site area is approximately 0.99ha and is currently a brownfield.

The site falls from southwest to northeast ranging in level from 86.5 mOD in the southwest to 83.49 mOD in the northeast. There is a single access to the subject site from Carmanhall Road. There is also a single access to the adjoining former Tack Packaging site from Ravens Rock Road.

## 2.3 Proposed Development

The proposed development consists of **334** Build to Rent residential apartment units within 4 No. apartment blocks and as follows:

- 79 No. Studio
- 175 No. 1 bed
- 80 No. 2 bed
- All residential units provided with private balconies/terraces to the north/south/east and west elevations Crèche 272 sqm.
- Residential amenity spaces 893 sqm. (including resident's gym, business centre, multipurpose room, staff facilities, multimedia/cinema room, shared working space, concierge and games room)
- Height ranging from 5 to 16 storeys (over basement)
- Landscaped communal space in the central courtyard
- Provision of a new vehicular entrance from Ravens Rock Road and egress to Carmanhall Road
- Provision of pedestrian and cycle connections
- 125 No. Car Parking, 6 No. Motorcycle Parking and 447cycle spaces at ground floor/under croft and basement car park levels
- Plant and telecoms mitigation infrastructure at roof level

THE CHASE BUSSINESS CENTER

CARMANHALL ROA

CARMANHALL ROA

STORE

BLOCK D

RECOKE

BLOCK D

RECOKE

R

The development also includes 2 no. ESB substations, lighting, plant, storage, site drainage works and all ancillary site development works above and below groundFigure 2-2 Proposed Site Layout

The existing ground levels around the site range from 86.5 m - 83.5 m OD. The ground floors of the proposed buildings step across the site to mimic the existing levels as far as reasonably practicable to minimise cut and fill across the site.

THREE ROCK PLAZA

## 2.4 Contiguous Development

A concurrent development with a separate Engineering Assessment on the former Tack Packaging site to the west will comprise 207 Build-to-Rent residential units and 79 car parking spaces at Lower Ground Level and Basement. Cycle parking with 288 spaces will be provided at Lower Ground Level. Access is proposed from Ravens Rock Road with egress onto Carmanhall Road.

The foul and surface water disposal, as well as water supply arrangements from this adjoining development will be separate from those serving the subject site.

## 3. Foul Water Drainage

## 3.1 Receiving Environment

There is an existing 225 mm Ø foul sewer located adjacent to the site along Carmanhall Road. There is also a 225mm Ø foul sewer along Blackthorn Road to the east of the subject site. Details of the adjacent foul sewer are shown in Appendix A – Irish Water Record Maps.

The foul sewer receiving environment for the proposed development consists of the 225mm foul sewer within Arkle Road as required by Irish Water.

Waterman Moylan drawing No's 21-118-P221 show the proposed foul water sewer network for the subject site.

It is proposed to drain the subject site to the existing 225mmØ foul sewer network on Arkle Road the northeast of the subject lands. It is important to note that the Avid Site (subject site under this planning application) will discharge foul water independently from the adjacent site, Tack Site. However, the attached Irish Water Confirmation of Feasibility received assesses the cumulative impact of the development of the 2 No. sites as set out in the Irish Water Pre-Connection Enquiry. In summary, Irish Water Stated that a foul connection to the Irish Water network at the premises is feasible without infrastructure upgrade by Irish Water. However, the foul connection has to be made to the Arkle Road network as shown below and in Waterman Moylan drainage drawing 21-118-P221.

SOTISMENT SOTISM

Figure 3-1 Location to Foul network required by Irish Water

## 3.2 Irish Water Pre-connection Enquiry Response

A pre-connection inquiry was submitted to Irish Water in November 2021 in respect of the foul connection from the proposed development. Subsequently, Irish Water has confirmed that based on the size of the proposed development and on the capacity currently available, that subject to a valid connection agreement being put in place, the proposed connection to the Irish Water network can be facilitated.

The Irish Water Pre-Connection Enquiry Form Response Letter (Ref. No. CDS21008079) dated 25 January 2022 is attached in Appendix B of this report. A set out above, it is important to note that the Avid Site (subject site under this planning application) will discharge foul water independently from the adjacent site, Tack Site. However, the attached Irish Water Confirmation of Feasibility received assesses the cumulative impact of the development of the 2 No. sites as set out in the Irish Water Pre-Connection Enquiry. In summary, Irish Water Stated that a foul connection to the Irish Water network at the premises is feasible without infrastructure upgrade by Irish Water. However, the foul connection has to be made to the Arkle Road network as shown above in figure 3-1 and in Waterman Moylan drainage drawing 21-118-P221.

## 3.3 Irish Water Statement of Design Acceptance

The foul and water supply design for the proposed development was submitted to Irish Water. Subsequently, Irish Water issued a letter of design acceptance stating that there are no objections to the proposals. A copy of the letter has been included in Appendix C.

## 3.4 Proposed Foul Water Drainage

The proposed development will consist of 334 No. residential units and 1 No. Creche. Based on the Irish Waters Code of Practice, the calculation of the peak foul flow from the proposed development has been determined as per Tables 1 and 2 below.

Table 1 Calculation of Proposed Foul Water Flow

Description	No. of Units	Flow I/h/day	Population per Unit	Infiltration Factor	Total Discharge
Residential Units	334	150	2.7	1.1	148,797
Creche	1	50	73	1.1	4,015
			62 pupils		
			11 staff		
				Totals	152,812 I/d

Table 2 Calculation of Proposed Peak Foul Flow

Calculation of Proposed Peak Foul Flow		Units
Dry Weather Flow Residential (DWF)	1.722	l/s

Dry Weather Flow Commercial (DWF)	0.046	I/s
Peak Foul Flow Residential (=6 x DWF)	10.33	l/s
Peak Foul Flow Commercial (=4.5 x DWF)	0.21	l/s
Total Peak Foul Flow	10.54	I/s

Waterman Moylan Drawing's 21-118-P221 illustrate the proposed layout for the foul water sewer outfall for the subject site.

## 3.5 Network Design

Foul Water Drains will be uPVC to Irish Water specification or concrete socket and spigot pipes (to IS 6).

Drains will be laid to comply with the Building Regulations 2010, and in accordance with the recommendations contained in the Technical Guidance Documents, Section H.

Foul water sewers will consist of uPVC or concrete socket and spigot pipes (to IS 6) and will be laid strictly in accordance with Irish Waters code of practice for Wastewater Infrastructure and Irish Water requirements for taking in charge.

All manholes will be constructed in block work, precast or cast in-situ concrete. Construction details for the proposed drainage systems are included in the accompanying planning submission drawing.

## 4. Surface Water Drainage

#### 4.1 Introduction

The following section deals with surface water drainage design including details of the SuDS measures proposed as part of the development.

The Surface Water Drainage design and SUDS Assessment carried out in the following sections has been undertaken in compliance with the requirements of the DLRCC County Development Plan 2022-2028, the guidelines set by the Greater Dublin Strategic Drainage Study (GDSDS) and CIRIA documents.

There is an existing 450mm diameter surface water sewer along Carmanhall Road continuing along Blackthorn Road. There is also a 375mm diameter surface water sewer along Blackthorn Road continuing along Burton Hall Road. The site will connect into the surface water manhole at the crossing of Carmanhall with Blackthorn Road to the northeast of the subject site. Refer to Appendix A for the existing surface water record map.

The existing site currently drains surface water, unrestricted, to the surface water sewer located on Blackthorn Road to the east of the site. It is proposed that the development will attenuate the surface water on-site before discharging at the existing greenfield rate.

The existing run-off rate for the existing hardstanding areas on site was estimated for the 1 in 1, 1 in 30 and 1 in 100 year return periods using the modified rational method:

 $Q = 2.78 \times A \times I$  (where A is the total pre-development area being drained in Hectares and I is the rainfall intensity in mm/h as estimated for the 60min storm from Flow using Met Eireann Data)

A = 0.49 ha (current hardstanding as measured from topographical survey)

I – 1 year return period = 11.235 mm/h

30 year return period = 27.335 mm/h

100 year return period = 43.042 mm/h

Table 3 Existing Run-off Rates for impermeable areas

Rainfall Event	Existing development run-off (I/sec) – Hardstanding Areas
Q1	2.78 x 0.49 x 11.235 = <b>15.30</b>
Q30	2.78 x 0.49 x 27.335 = <b>37.24</b>
Q100	2.78 x 0.49 x 43.042 = <b>58.63</b>

#### 4.2 Site Characteristics

The following parameters have been used in greenfield run-off rate and attenuation calculations.

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Table 4 Surface Water Catchment Details

	Catchment
Site Area (Catchment) - Ha	0.73 (net of surrounding verges)
Hardstanding – Ha	0.60
SAAR – mm*1	930
SOIL Index*2	0.37
Climate Change	30%

<sup>\*1 -</sup> From Met Éireann data.

\*2 – The soil type of Ireland indicated Soil Type 1. Furthermore a Site investigation was carried out in February 2021 on the proposed site. The results of the site investigation revealed there is no infiltration present on the site. These soil conditions are expected for Soil type 3 and therefore 0.37 is used as Soil Index for this site. Refer to Appendix D for the above-mentioned Site Investigation.

The site investigation also revealed a highwater table is present at the site. The highest groundwater table was recorded as 1.63 - 2.5 m bgl (below ground level), in June 2020, four months after installation of the standpipes.

#### 4.3 Greenfield run-off rates

The Local Authority requirements are that post-development run-off rates are limited to greenfield run-off rates for the site. The greenfield run-off rates for the site have been calculated in accordance with the Institute of Hydrology report No 124 "Flood Estimation for Small Catchments", using the UK SUDS Website. Based on a total hardstanding of 0.6 Ha, the Greenfield run-off for the site is 2.4 l/s (Qbar). Please refer to Appendix E.

#### 4.4 SuDS Assessment

As per Dun Laoghaire County Council guidelines surface water should be managed in accordance with the Greater Dublin Strategic Drainage Study (GDSDS) Regional Drainage Policies Volume 6, for New Developments and CIRIA documents. These documents specify that surface water run-off should be managed as close to its source as possible, with the re-use of rainwater within the buildings prioritised.

Sustainable Urban Drainage Systems (SUDS) have been developed and are in use to alleviate the detrimental effects of traditional urban storm water drainage practice that typically consisted of piping run-off of rainfall from developments to the nearest receiving watercourse. Surface water drainage methods that take account of quantity, quality and amenity issues are collectively referred to as SUDS. They are typically made up of one or more structures, built to manage surface water run-off. The use of SUDS to control run-off also provides the additional benefit of reducing pollutants in the surface water by settling out suspended solids, and in some cases providing biological treatment.

A stormwater management or treatment train approach ensures that run-off quantity and quality is improved. The following objectives of the treatment train provide an integrated and balanced approach to

help mitigate the changes in stormwater run-off flows that occur as land is urbanised and to help mitigate the impacts of stormwater quality on receiving systems:

- 1) Source control: conveyance and infiltration of run-off; and
- 2) Site Control: reduction in volume and rate of surface run-off, with some additional treatment provided.

The applicant has considered the use of all appropriate SUDS measures as part of the site SUDS strategy, details are outlined in Table 5 below.

Table 5 SuDs Measures

SUDS Stage	SUDS Measure	Measure Outline	Use on Site
Source Control	Permeable Asphalt	Permeable pavements are alternative paving surfaces to standard finishes that allow stormwater run-off to filter through voids in the pavement surface into an underlying stone reservoir, where it is temporarily stored and/or infiltrated. Permeable asphalt is very effective at removing a wide range of pollutants from surface water runoff as they are either retained on the pavement surface or flushed into the granular subbase where they become trapped and are degraded over time.	Permeable asphalt will be utilised for the surface of footpath to the west of the site to provide treatment and storage to rainwater falling on these areas and part of the rainwater falling into the main road.  As described above, the ground conditions are not considered suitable for infiltration and the groundwater table was found at high level. Therefore, the permeable paving would be lined with an impermeable geotextile membrane due to the lack of infiltration available on the site and to prevent groundwater ingress.  The design will include a perforated pipe to convey surface water to the site wide drainage system.
	Green Roofs/ Green Podium	As well as providing ecological benefits, green roofs contribute the following positive effects to surface water drainage design:  • The retention of water, through storage in the growing medium and evapotranspiration from the	The locations of the green roofs are illustrated on the accompanying Waterman Moylan Drawing 21-118-P225 - SUDS Measures and overland flood route. Refer to section 4.5 of this report for further details on the Green Roof proposals for this development.

	roof's plants and substrate, reducing run-off volumes and the burden on the drainage network.  • Due to the time for water to infiltrate and permeate the substrate, there is also a reduction in peak rates of run-off, helping to reduce the risk of flooding.  • They improve water quality through the filtration of pollutants during the process of water infiltration. This provides treatment in line with CIRIA SuDS Manual management train.  Although green roof space can reduce peak flow rates in the small storm events and aid in reducing the volume of run-off from the site, they operate as conventional roofs in higher storm events. Therefore, green roofs cannot be considered in the surface water drainage run-off calculations for the development. As stated in CIRIA C697 "although green roofs absorb most of the rainfall that they receive during ordinary events, there is still the need to discharge excess water to the building's drainage system. This is because their hydraulic performance during extreme events tends to be fairly similar to standard roofs."	
Filter Drains	Filter Drains are shallow trenches filled with gravel and wrapped in a geotextile membrane to treat and temporarily store surface water runoff.	Filter Drains are provided for the footpath to the north of the site to treat surface water at source before conveying it to the site wide surface water drainage network.

	SUDS Measure	Measure Outline	Use on Site
SUDS Stage	Attenuation Tank and Hydro-brake	Attenuation tanks are used to create a below ground void space for the temporary storage of surface water before controlled release to the stream.	It is proposed to use a concrete attenuation tank to store surface water on site before discharging to the public surface water sewer via a hydro-brake.
		Hydro-brakes are used to restrict the outfall from the attenuation tank to the equivalent of the existing agricultural run-off. This ensures the development will not give rise to any impact downstream of the site.	
Site Control	Petrol Interceptor	A petrol interceptor is a trap used to filter out hydrocarbon pollutants from rainwater run-off. It is typically used in road construction to prevent fuel contamination of water courses carrying away the run-off.	Two petrol Interceptors will be installed, upstream of the proposed Attenuation tank as a final treatment level before discharging to the attenuation tank.
		Petrol interceptors work on the premise that some hydrocarbons such as petroleum and diesel float on the top of water. The contaminated water enters the interceptor typically after flowing off roads and entering a drain before being deposited into the first tank inside the interceptor. The first tank builds up a layer of the hydrocarbon as well as other scum preventing it from entering the water course.	
	Bio-retention tree pits	These tree pits are engineered pits that allow for the drainage through and retention of water within the tree pit. In some cases, the tree pit is retained by a pre-cast concrete structure. In others, polymer-based support structure, within the root zone of the tree is used, which can also provide for additional aeration. Aeration of the subsoil and overflow drainage pipework within the pit is provided or an adjacent road gully,	It is proposed to incorporate tree pits to the south of the development to provide interception storage to the south access road.

	downstream of the inlet to the tree pit is used.	
Rain garden	Rain gardens are typically small systems that serve part of a single property. Filter and drainage layers are generally replaced by a thin layer of compost/sand-amended native soils or specified soil mixes (engineered soils). They have a simple inflow where rainwater enters the garden, and they have maximum depth of standing water of 150mm. They can have an above-ground overflow where excess water exits, although in some instances a simple underdrain may be more effective than providing a small control structure.	It is proposed to incorporate rain gardens to the east of the development to provide a better surface water quality runoff of the development. The rain gardens will be connected to the wider surface water network and attenuated to the attenuation tank located at basement level.

## 4.5 Green Roof Policy

Green Roofs have been considered and incorporated into the development proposals in accordance with Appendix 7.2 of DLRCC County Development Plan 2022-2028. There are 5 No. Green Roof Policy standards, all of which have been considered for this planning application as follows:

## Standard GR1-Applicable development types

Planning applications which include roof areas of greater than 300 square metres for the following development types must make provision for a green and/ or blue roof (which includes a green component) as part of the development proposals.

- Apartment Developments
- Employment Developments
- · Retail and Ancillary Shopping
- Leisure Developments
- Education Facilities

The proposed development has 4 No. apartment blocks and therefore green roof must be incorporated into the design. The locations of the green roofs are illustrated on the accompanying Waterman Moylan drawing 21-118-P225 - SUDS Measures and overland flood route.

#### Standard GR2 – Aerial Coverage

To maximise the provision for biodiversity, green roofs must meet the following coverage requirements for all applicable buildings within the application boundary, subject to a reasonable allowance being made for the provision of services at roof level.

Table 6 Minimum Green Roof Coverage (Appendix 7.2 DLRCC Development Plan 2022-2028)

Type of Green Roof	Minimum Coverage (% of Total Roof Area being developed)
Extensive	70%
Intensive	50%

As described in the DLRCC Green Roof Policy document, the are two main types of green roof:

- **Extensive** green roofs are more lightweight when compared with intensive green roofs with a shallow soil layer and are not normally designed to provide access for people.
- Intensive green roofs have a deep layer of soil, which can support a range of plants, trees and shrubs. Native species (plants which would grow naturally in the local area) can provide a rich habitat for wildlife. Intensive Green Roofs can be designed to include access for people.

Extensive roofs are defined having a minimum substrate depths of 80mm and Intensive roofs are defined as having a substrate minimum depth of 200mm (Source; the GRO Green Roof Guide).

The proposed development will comprise a mix of Extensive and Intensive green roofs. The exact location for each type of green roofs will be fully designed at detail design stage. For the purpose of this application, 82.8% Green Roof will be provided and the location of Green Roof is indicated on Waterman Moylan Drawing 21-118-P825 - SUDS Measures and overland flood route.

### Standard GR3 – Hydraulic Requirements

Where the green/blue roof provides attenuation and management of storm runoff the applicant should demonstrate

- Compliance with the Greater Dublin Strategic Drainage Study 2005 (GDSDS) Criterion 1-4.
- Provision for climate change allowance and urban creep as appropriate.
- Provision for overflow and exceedance as part of the drainage design.

It is not proposed to provide attenuation within the proposed Green Roofs. Although green roof space can reduce peak flow rates in the small storm events and aid in reducing the volume of run-off from the site, they operate as conventional roofs during higher storm events. Therefore, green roofs cannot be considered in the surface water drainage run-off calculations for the development. As stated in CIRIA C697 "although green roofs absorb most of the rainfall that they receive during ordinary events, there is still the need to discharge excess water to the building's drainage system. This is because their hydraulic performance during extreme events tends to be fairly similar to standard roofs."

#### Standard GR4 - Design in accordance with best practice Industry guidance

Designs for green and blue roofs should demonstrate that the designer has applied an abundance of caution as part of the design process and that designs are in adherence with current best practice design guidance.

The green roof will be designed at detail design stage by a green roof specialist designer with a good reputation within the industry. The developer will ensure that designs are in adherence with current best practice design guidance.

#### Standard GR5 – Design for access, operation and maintenance

Green and blue roof designs should be designed to ensure that any required maintenance or operation activities can be undertaken in a safe and cost-effective manner.

A Maintenance and Operation Manual will be provided by the green roof manufacturer to the Management company to ensure proper and safe operation of the Green Roofs. Refer to Table 14 below for the proposed green roof maintenance schedule.

Access to each of the green roofs is crucial not only for installation and ongoing maintenance but also for bringing up materials, soils and plants in a safe manner. Access to the green roof is provided from the access hatches for all the Blocks. Specific access for each of the Green Roofs is shown in the accompanying architect's drawings.

#### 4.6 Stormwater Calculations

The total impermeable area of the catchment including roads, car-parking and roofs, is approximately 0.6 Ha, and the peak outflow will be limited to 2.4 l/s in the 1 in 100-year event. The 1 in 100 year critical design storm plus an additional 20% for climate change has been used for storm water attenuation calculations and a storage volume requirement of 423 m³ is determined. A total volume of 553 m³ will be provided in a concrete tank located beneath the podium at the car parking level. The calculation for the storage design is included in Appendix F. The proposed surface water drainage network is indicated on Waterman Moylan drawings 21-118-P220 and P222.

### **Urban Creep Factor**

The new DLRCC Development Plan 2022-2028 states that all development must apply a 1.1 factor to the drainage design and attenuation volumes to accommodate urban creep. Urban creep factor considerers the potential impact on the drainage system from exempted development such as small extensions to houses or paving over front gardens to create driveways. The proposed development is comprised of apartment blocks and therefore it will be fully managed by a Management Company. Residents will not be able to change hardstanding areas for the site and therefore there is no need to apply an urban creep factor for this development. This has been agreed with John Cunniffe from DLRCC and email can be found in Appendix G.

## 4.7 Network Design

As described above, the proposed surface water drainage system for this development has been designed as a SUDS system and uses permeable paving, filter strips and green roofs/podium, below ground attenuation together with flow control devices and petrol interceptor to treat run-off and remove pollutants to improve quality, restrict outflow and control quantity.

Strict separation of surface water and wastewater will be implemented within the development. Surface water local drains will be a minimum of 225mm dia. and generally will consist of PVC (to IS123) or concrete socket and spigot pipes (to IS 6). These drains will be laid to comply with the requirement of the Building Regulations 2010, and in accordance with the recommendations contained in the Technical Guidance Documents, Section H and will be laid strictly in accordance with the requirements of Dun Laoghaire Rathdown County Council.

### 4.8 Interception Storage

Interception storage is defined in the SuDS Manual as "the capture and retention on site of the first 5mm of the majority of rainfall events". In accordance with the table 24.6 of the SuDS Manual CIRIA C753 the following guidelines have been used in calculating the area of the site benefiting from interception storage;

Table 7 Interception Mechanisms (Table 24.6 The SuDs Manual)

Systems	Interception methods assumed compliant for zero runoff from the first 5mm of rainfall for 80% of events during the summer and 50% in winter.	
Green Roofs/podium	All surfaces that have green roofs/podium.	
Permeable Paving	All permeable pavements, whether lined or not, can be assumed to comply, provided there is no extra area drained to the permeable pavement.	
	Where the pavement also drains an adjacent impermeable area, compliance can be assumed for all soil types where the pavement is unlined, as long as the extra paved area is no greater than the permeable pavement area	
Filter strips	Roads drained by filters strips, where the longitudinal gradient of the vegetated area is less than 1:100, are suitable for Interception delivery for impermeable surface areas up to 5 times the base of the vegetated surface area receiving the runoff. Components steeper than 1 in 100 cannot be deemed to provide Interception unless additional effective Interception design can be demonstrated.	

As described in section 4.4 and 4.5 the proposed development will provide, Green Roofs, green podium, filter drains and permeable paving. In order to calculate the percentage area of site benefiting from each form of interception storage the site areas are described in Table 8 below and demonstrated on Waterman Moylan drawing 21-118-P225.

At Podium level, all the hardstanding areas will be discharged into the landscape areas. The design will include a perforated pipe to convey surface water to the surface water network at ground level in order to discharge and attenuate water into the attenuation tank.

Table 8 Interception Storage Provided

Area	Total Hardstanding Area m2	Interception mechanism	Interception Area m2	green roof %	Percentage Benefiting %
Roof Blocks D-E- F-G	3207.0	Green Roof	2468.8	77.0	77.0
Podium Level	1647.0	Green podium	1647.0	N/A	100.0
Main Road		Porous Asphalt	844.4	N/A	
and	1070.2	Filter strips	83.7	N/A	140.8
Footpaths		Raingardens/Bioretention Tree pits	579.0	N/A	
TOTAL	5924.2		5622.9	N/A	94.9

Within the basement carpark area, any rainwater entering the system as a result of snow melt or raindrops from cars will pass through a petrol interceptor providing treatment and will be discharged into the foul water network.

## 5. SuDS Maintenance

For the SuDS strategy to work as designed it is important that the entire drainage system is well maintained. It will be the responsibility of the site management team to ensure the drainage system is maintained. Maintenance and cleaning of gullies, drain manholes (including catch pits) and attenuation tanks will ensure adequate performance. The recommended program is outlined in the tables below.

Table 9 Concrete Attenuation Tank Maintenance Schedule

SUDS Element	Maintenance				
	Maintenance Issues				
	Maintenance Period	Maintenance Task	Frequency		
S.		Inspect and identify any elements that are not operating correctly. If required, take remedial action.	Monthly for three months, then annually		
Attenuation Tanks	Regular	Remove sediment/debris from catchment surface that may lead to blockage of structures.	Monthly or as required		
nuati		Remove sediment/debris from catch pits/ gullies and control structures.	Annually, after severe storms or as required		
Atte	Remedial Work	Repair inlets, outlets, vents, overflows and control structures.	As required		
	Monitoring	Inspect all inlets, outlets, vents, overflows and control structures to ensure they are in good condition and operating as designed.	Annually or after severe storms		
		Survey inside of tank for sediment build-up and remove if necessary	Every five years or as required		

Table 10 Permeable Paving Maintenance Schedule

SUDS Element	Maintenance				
	Maintenance period	Maintenance Task	Frequency		
aving	Regular	Brushing and vacuuming (standard cosmetic sweep over whole surface)	Once a year, after autumn leaf fall, or as required, based on site specific observations of clogging or manufacturer's recommendations.		
<u>ө</u>	Occasional	Removal of weeds	As required		
Permeable Paving	Remedial work	Remediation work to any depressions, rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users	As required		
	Monitoring	Inspect silt accumulation rates and establish appropriate brushing frequencies	Annually		
		Monitor inspection chambers	Annually		

Table 11 Filter Strip Maintenance Schedule

Maintenance period		Maintenance Task	Frequency
		Remove the litter and debris	Monthly, or as required
		Cut grass – to retain height within specified design range.	Monthly (during growing season), or as required
Filter Strips	Regular	Manage other vegetation and remove nuisance plants.	Monthly at start, then as required
		Inspect inlets, outlets and overflows for blockages, and clear if required.	Monthly
		Inspect infiltration coverage	Monthly for 6 months, quarterly for 2 years, then half yearly
		Inspect inlets and facility surface for silt accumulation, establish appropriate silt removal frequencies	Half yearly
	Occasional	Reseed areas of poor vegetation growth, alter plant types to better suit conditions, if required	As required or if soil is exposed over 10% or more of the swale treatment area

		Repair erosion or other damage by returfing or re-seeding	As required
		Re-level uneven surfaces and reinstate design levels	As required
	Remedial actions	Remove build-up of sediment on upstream gravel trench, flow spreader or at top of filter strip	As required
		Remove and dispose of oils or petrol residues using safe standards practices	As required

Table 12 Bio-retention Tree Pits Maintenance Schedule

	Maintenance Period	Maintenance Task	Frequency
		Remove the litter and debris	Monthly, or as required
		Manage other vegetation and remove nuisance plants.	Monthly at start, then as required
Tree Pits	Regular	Inspect inlets and outlets for blockages, and clear if required.	Monthly
		Inspect inlets and facility surface for silt accumulation, establish appropriate silt removal frequencies	Half yearly
	Occasional	Check Tree Health and manage Tree appropriately	Annually
		Remove silt build-up form inlets and surface and replace mulch as necessary	Annually, or as required
		Water	As required (in periods of drought)
	Monitoring	Inspect all silt accumulation rates and establish appropriate removal frequencies.	As required

Table 13: Rain gardens Maintenance Schedule

Maintenance Period		Maintenance Task	Frequency
		Remove the litter and debris	Monthly, or as required
	Regular	Manage other vegetation and remove nuisance plants.	Monthly at start, then as required
Rain gardens		Inspect inlets and outlets for blockages, and clear if required.	Monthly
		Inspect inlets and facility surface for silt accumulation, establish appropriate silt removal frequencies	Half yearly
	Occasional	Check Garden Health and manage Garden appropriately	Annually
		Remove silt build-up form inlets and surface and replace mulch as necessary	Annually, or as required
		Water	As required (in periods of drought)
	Monitoring	Inspect all silt accumulation rates and establish appropriate removal frequencies.	As required

Table 14 Green Roof/podium Maintenance Schedule

SUDS Element	Maintenance				
	Maintenance Issues	Vegetation becoming either overgrown or dying			
⊑	Maintenance Period	Maintenance Task	Frequency		
n Roof/podiu	Period  Inspect all components including soil substrate, vegetation, drains, membranes and roof structure for proper operation, integrity of waterproofing and structural stability		Annually and after severe storms		
Green		Inspect soil substrate for evidence of erosion channels and identify any sediment source	Annually and after severe storms		
		Inspect drain inlets to ensure unrestricted run-off from the drainage	Annually and after severe storms		

Regular	layer to conveyance or roof drain system.	
	Inspect underside of roof for evidence of leakage.	Annually and after severe storms
	Remove debris and litter to prevent clogging of inlet drains and interference with plant growth.	Six monthly and annually or as required
	During establishment (i.e. year one), replace dead plants as required.	Monthly
	Post-establishment, replace dead plants as required (where >5% of coverage)	Annually (in autumn)
	Remove fallen leaves and debris from deciduous plant foliage	Six monthly or as required
	Remove nuisance and invasive vegetation, including weeds	Six monthly or as required
	Mow grasses, prune shrubs and manage other planting (if appropriate) as required – clippings should be removed and not allowed to accumulate.	Six monthly or as required
Remedial Work	If erosion channels are evident, these should be established with extra soil substrate similar to the original material, and sources of erosion damage should be identified and controlled	As required
	If drain inlet has settled, cracked or moved, investigate and repair as appropriate	As required

## 6. Benefits to the Surrounding Existing Drainage Network

It is important to note the very significant benefit the proposed development will have on the existing drainage network. The site currently discharges surface water, unrestricted to the public stormwater sewer. The proposed development will significantly reduce the surface water run-off to the existing public drainage network as demonstrated in Table 15 below. The introduction of the SUDS measures outlined earlier will also improve the quality of the discharge.

Table 15 Surface Water Run-off rates

Rainfall Event	Existing development run-off (I/sec)	Proposed run-off (I/sec)	Difference (%)
Q1	15.30 l/s	2.4 l/s	-84.31 %
Q30	37.24 l/s	2.4 l/s	-93.55 %
Q100	58.63 l/s	2.4 l/s	-95.9 %

## 7. Water Supply

## 7.1 Water Supply – General

There is an existing watermain connection to the west of the site. This is a 101.6mm Asbestos pipe into the existing 6 inch Asbestos watermain that runs along Blackthorn Road to the east of the site. It is proposed to connect the subject site to the 6 inch Asbestos watermain along Blackthorn Road as per the current existing connection.

It is important to note that the Avid Site (subject site under this planning application) will be connected to the existing public watermain independently from the adjacent site, Tack Site. However, the attached Irish Water Confirmation of Feasibility received assesses the cumulative impact of the development of the 2 No. sites, stating that subject (Avid) site will need to be connected to the 6 inch diameter Asbestos main along Blackthorn Road and to the 14 inch diameter Asbestos main along Carmanhall Road. The adjacent (Tack) site also connects to the 14 inch diameter Asbestos main along Carmanhall Road

A Pre-Connection Enquiry form was submitted to Irish Water in November 2021 which outlined the proposals for the water supply to the development to the north of the subject lands. Irish Water advised that two water connections to the public main are feasible without infrastructure upgrade by Irish Water. These connections would be to the 14 inch diameter Asbestos main along Carmenhall Road and to the 6 inch Asbestos main along Blackthorn Road.

The water demand for the proposed development is calculated according to the Irish Water Code of Practice and is set out in Table 13 below.

Table 16 Total Water Demand

Description	No. of Units	Flow I/h/day	Population per Unit	Total Demand (I/d)
Residential Units	334	150	2.7	135,270
Crèche	1	50	73	3,650
			62 pupils	
			11 staff	
Total				138,920 I/d

The total water requirement from the public supply, for the development, is estimated at 139 m<sup>3</sup>/day.

Waterman Moylan Drawing 21-118-P250 shows the proposed indicative water supply layout for the subject site.

### 7.2 Irish Water Pre-Connection Enquiry

As set out above a pre-connection inquiry was submitted to Irish Water in November 2021 in respect of the foul connection from the proposed development. Subsequently, Irish Water has confirmed that based on the size of the proposed development and on the capacity currently available, that subject to a valid

connection agreement being put in place, the proposed connection to the Irish Water network can be facilitated.

The Irish Water Pre-Connection Enquiry Form Response Letter (Ref. No. CDS21008079) dated 25 January 2022 is attached in Appendix B of this report. A set out above, it is important to note that the Avid Site (subject site under this planning application) will obtain a water supply independently from the adjacent site, Tack Site. However, the attached Irish Water Confirmation of Feasibility received assesses the cumulative impact of the development of the 2 No. sites as set out in the Irish Water Pre-Connection Enquiry. In summary, Irish Water has stated that a water connection to the public network can be facilitated without infrastructure upgrade by Irish Water. Irish Water requests in the Pre-Connection Enquiry response letter that the Water Supply connections are made to the 14 in Asbestos main to the North of the site and a second connection is feasible to the 6 inc Asbestos main to the East of the site. These two connections are shown below in green and red respectively and in Waterman Moylan drawing 21-118-P250.



Figure 7-1 Water Supply connection locations requested by Irish Water.

## 7.3 Irish Water Statement of Design Acceptance

The foul and water supply design for the proposed development was submitted to Irish Water. Subsequently, Irish Water issued a letter of design acceptance stating that there are no objections to the proposals. A copy of the letter has been included in Appendix C.

## 8. Transport

A site-specific Transport and Traffic Assessment (T&TA) has been carried out by Waterman Moylan. This is included under separate cover as part of this application. A summary of the T&TA is included beneath.

#### **Proposed Development**

The proposed development will comprise some 334 Build-to-Rent residential units.

Car parking with a total of 125 car spaces including 7 car sharing spaces will be provided at Lower Ground and Basement. Access is proposed from Carmanhall Road with egress onto Blackthorn Road.

Cycle parking with 447 spaces will be provided at Lower Ground Level. Access is proposed from Blackthorn Road.

The public realm around the site will incorporate an upgrade of the pedestrian and cycle environment.

The development includes all associated infrastructure to service the development including access junctions, footpaths and cycle paths together with a network of watermains, foul water drains and surface water drains.

#### **Contiguous Development**

A concurrent development with a separate Traffic & Transport Assessment on the former Tack Packaging site to the west will comprise 207 Build-to-Rent residential units and 79 car parking spaces at Lower Ground Level and Basement. Access is proposed from Ravens Rock Road and egress onto Carmanhall Road.

The traffic impact from this contiguous development has been incorporated into the T&TA.

#### **Program**

At the time of writing in August 2022, it is likely that construction of the proposed development could commence in 2023 for completion in 2026.

Projections are included for Design Year 2031 (Opening Year + 5) and Future Year 041 (Opening Year + 15).

#### **Future Road and Cycle Schemes**

During the preparation of the T & TA, consultations were held with the project engineers for two future schemes in the area of the subject site. The two schemes which are being developed by Dun Laoghaire Rathdown County Council are: -

- (a) ESB Link Road Junction 14 Roundabout to Blackthorn Road.
- (b) Sandyford Business District Pedestrian and Cycle Improvement Scheme.

Both schemes and their impact on the road network in the area of the subject site are described in the T & TA.

Project Number: 21-118

Document Reference: 21-118r.069

It is understood at the time of writing in August 2022, that both schemes are progressing to the tender stage for completion in 2023.

#### DLR County Development Plan 2022 - 2028

The requirements of the DLR County Development Plan in relation to Sustainable Travel and Transportation including roads, car parking, cycling and walking are identified in this report and their application in relation to the proposed development clarified.

Likewise, the requirements of the Sandyford Urban Framework Plan in relation to Sustainable Infrastructure Policies and Objectives.

#### **Car Parking**

The proposed provision of car parking will be 125 spaces calculated at the rate of 0.375 space per unit per unit for 334 units.

The provision of 125 spaces will include 88 standard spaces, 25 spaces with charging facilities for electric vehicles (20%), 5 spaces for disabled drivers (4%) and 7 spaces for car sharing (GoCar).

Each car sharing spaces will be the equivalent of 20 standard spaces.

The effective provision of car parking at the proposed development would be the equivalent of 258 spaces comprising 118 standard spaces and 140 car sharing spaces compared to a maximum allowable provision of 278 spaces under the current Development Plan.

Compliance has also been demonstrated in the T &TA with Section 8.2.4.5 Car Parking Standards of the DLR County Development Plan 2022 – 2028 which provides for reduced car parking standards for any development (residential and non-residential) complying with certain criteria.

## **Public Transport - Luas**

The proposed development will be located adjacent to the Luas Green Line. The nearest Luas stops are Stillorgan and Sandyford both located on Blackthorn Avenue less than 0.5km to the north of the proposed development. Both stops are within 6 minutes walking distance.

Following completion of the Green Line Capacity Enhancement Scheme in 2019, the current capacity of the Green Line during the AM Peak is 6,300 passengers per hour in both directions compared to a peak loading of 4,648 passengers per hour inbound between Milltown and Cowper.

Based on a modal split of 28%, the peak demand from the proposed development is expected to be 344 passengers during the AM Peak of which 50% can be expected to travel during the AM Peak Hour. This demand of 172 passengers per hour is equivalent to 1.3% of the Green Line Capacity of 12,600 passengers per hour.

#### **Public Transport - Bus**

The combined development will be well served by stage bus services operated by a number of companies in the surrounding area. Bus stops are located on Burton Hall Road, Blackthorn Road, and Blackthorn Avenue less than 6 minutes' walk from the proposed development.

The projected demand for bus services during the AM Peak is some 110 passengers per hour. This demand is well within the capacity of the existing bus services being 6% of the capacity of 1,840 persons per hour provided on the bus services in the surrounding area.

#### **Traffic Impact**

During the preparation of the T & TA, two alternative scenarios were considered as part of the assessment of the traffic impact of this development.

Firstly, to assess the traffic impact of a residential development on the subject site.

Secondly, to assess the subject site in conjunction with the adjoining site as a single development for traffic purposes. For reasons of this latter option was selected and the developments on the two sites assessed as a single development on a single site.

The results of the assessment confirmed that the junctions on the surrounding road network would remain within in capacity post development in the Opening Year 2026 through the Design Year in 2031 to the Future Year 2041.

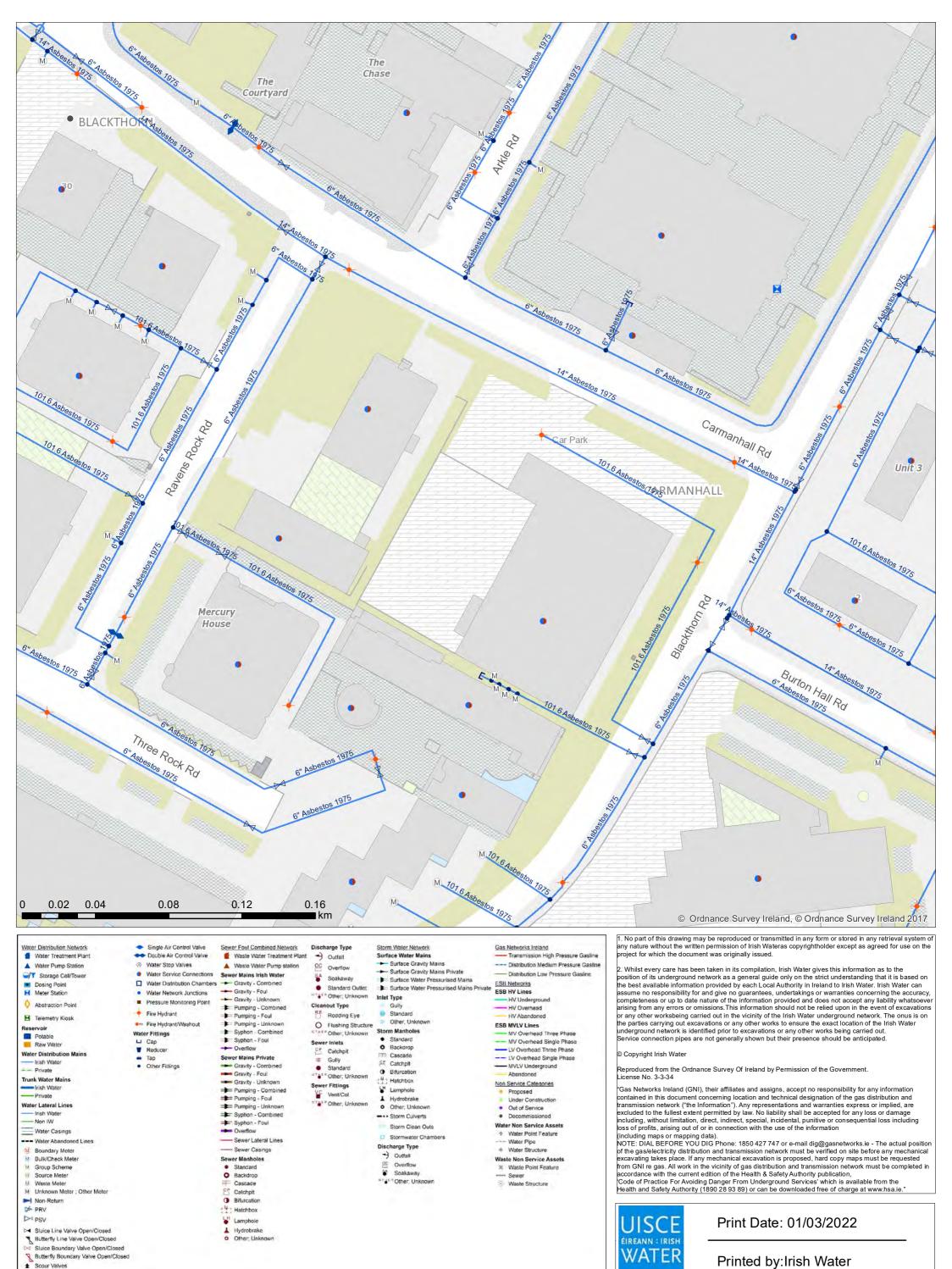
#### Summary

The T & TA demonstrates that the proposed development will be consistent with the objectives for Sustainable Travel and Transport set out in the DLR County Development Plan 2022 – 2028 and the Sandyford Urban Framework Plan 2022 - 2028.

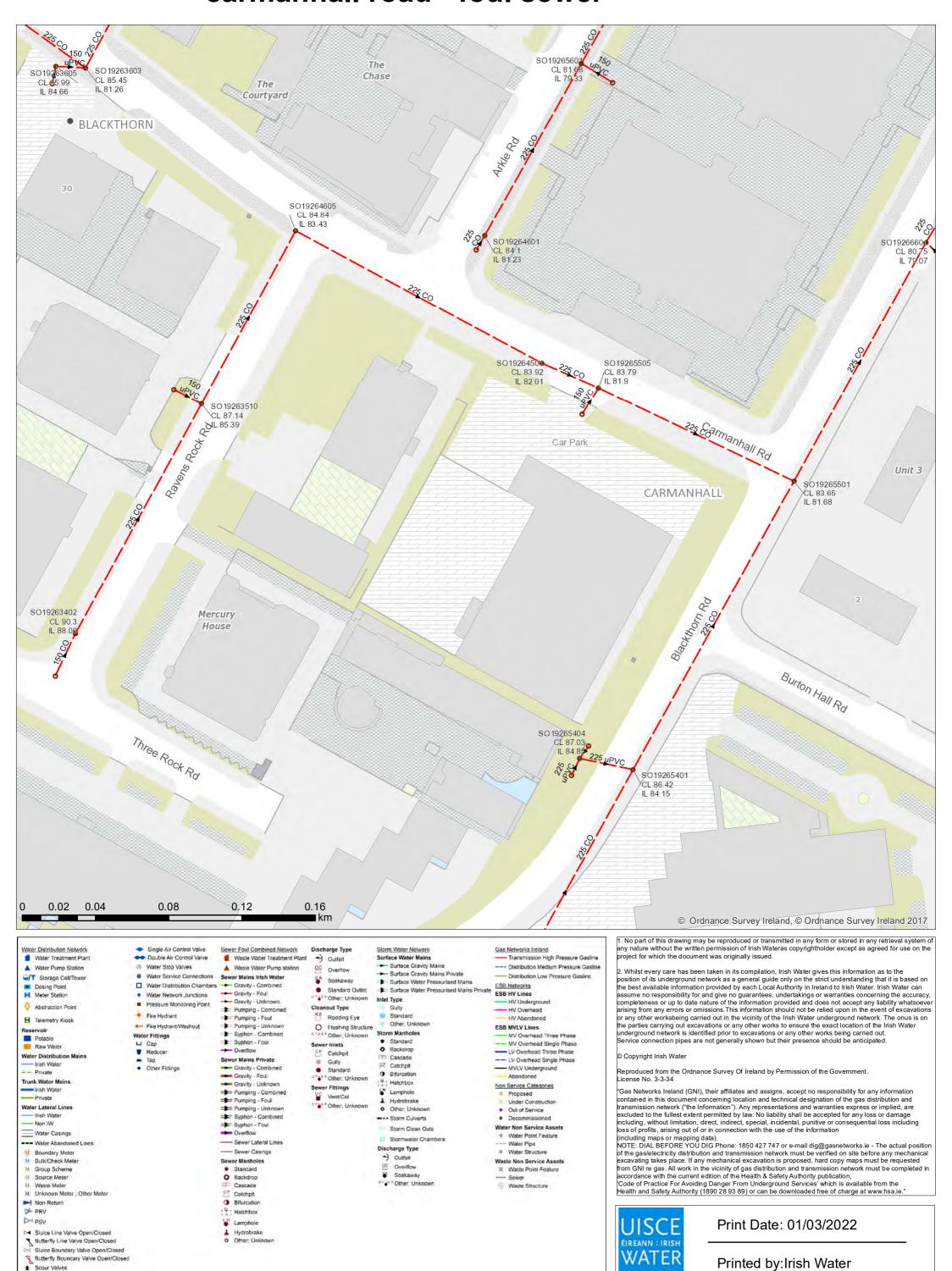
## **APPENDICES**

## A. Irish Water Records Map

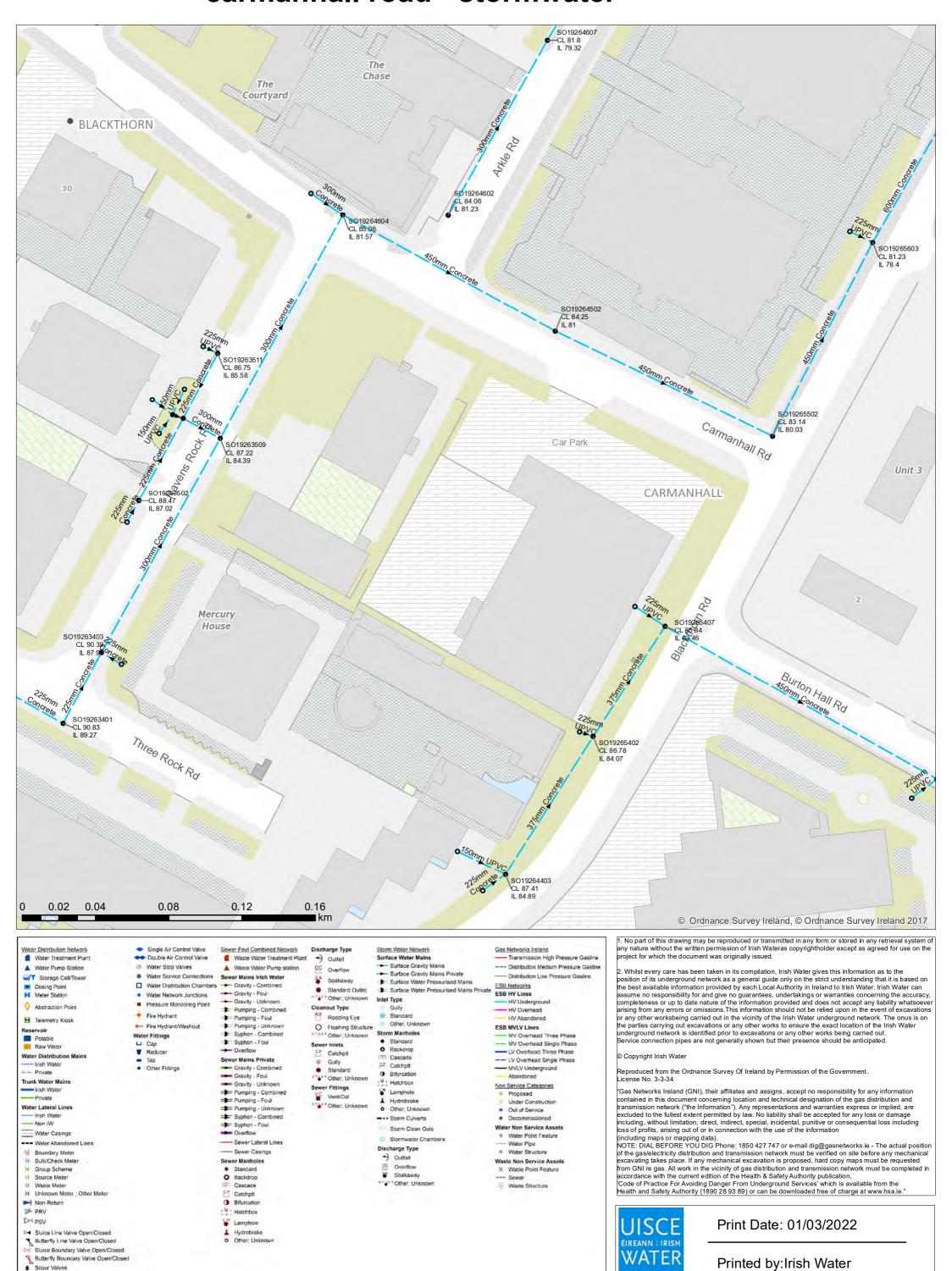
# carmanhall road - watermains



# carmanhall road - foul sewer



# carmanhall road - stormwater



**B. Irish Water Pre-Connection Enquiry Response** 



Jairo Rivero

Block S
Eastpoint Business Park
Alfie Byrne Road
Dublin
D03H3F4
Ireland

Uisce Éireann Bosca OP 448 Oifig Sheachadta na Cathrach Theas Cathair Chorcaí

Irish Water PO Box 448, South City Delivery Office, Cork City.

www.water.ie

25 January 2022

Re: CDS21008079 pre-connection enquiry - Subject to contract | Contract denied

Connection for Housing Development of 550 unit(s) at Ravens Rock Road, Sandyford, Dublin

Dear Sir/Madam,

Irish Water has reviewed your pre-connection enquiry in relation to a Water & Wastewater connection at Ravens Rock Road, Sandyford, Dublin (the **Premises**). Based upon the details you have provided with your pre-connection enquiry and on our desk top analysis of the capacity currently available in the Irish Water network(s) as assessed by Irish Water, we wish to advise you that your proposed connection to the Irish Water network(s) can be facilitated at this moment in time.

SERVICE	OUTCOME OF PRE-CONNECTION ENQUIRY  THIS IS NOT A CONNECTION OFFER. YOU MUST APPLY FOR A CONNECTION(S) TO THE IRISH WATER NETWORK(S) IF YOU WISH TO PROCEED.
Water Connection	Feasible without infrastructure upgrade by Irish Water
Wastewater Connection	Feasible without infrastructure upgrade by Irish Water
	SITE SPECIFIC COMMENTS
Water Connection	This Confirmation of Feasibility to connect to the Irish Water infrastructure does not extend to your fire flow requirements. Please note that Irish Water cannot guarantee a flow rate to meet fire flow requirements and in order to guarantee a flow to meet the Fire Authority requirements, you should provide adequate fire storage capacity within your development  Connection is feasible to the 14" Asbestos main (Green in below screenshot) to the North of the site. A bulk meter is to be installed on this connection.

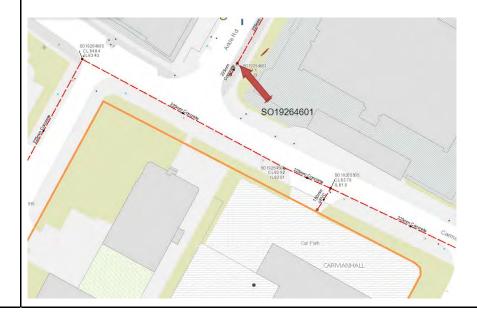
A second connection is feasible to the 6" Asbestos main (Red in below screenshot) to the East of the site. A control valve is to be placed on this main allowing for this connection to be set to closed during normal operations.



Separate storm and foul water connection services have to be provided for the Development. The surface and storm water from the site must be discharged only into an existing storm water network that does not discharge to an IW combined/foul sewer. The connection arrangement should be agreed with the Local Authority Drainage Division.

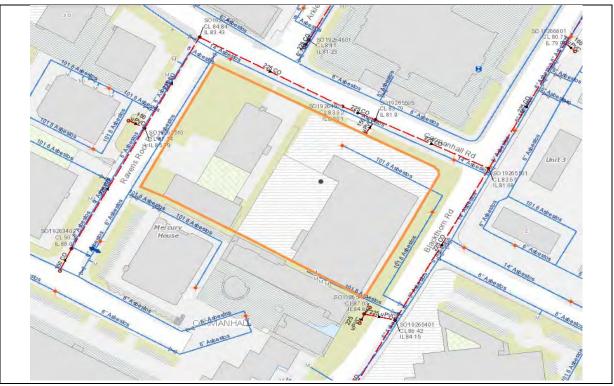
The connection has to be made to the Arkle Road (MH: SO19264601) network as shown below. A second connection to other sewers adjacent to the site are not feasible based on current constraints in the downstream network.

Wastewater Connection



The design and construction of the Water & Wastewater pipes and related infrastructure to be installed in this development shall comply with the Irish Water Connections and Developer Services Standard Details and Codes of Practice that are available on the Irish Water website. Irish Water reserves the right to supplement these requirements with Codes of Practice and these will be issued with the connection agreement.

#### The map included below outlines the current Irish Water infrastructure adjacent to your site:



Reproduced from the Ordnance Survey of Ireland by Permission of the Government. License No. 3-3-34

Whilst every care has been taken in its compilation Irish Water gives this information as to the position of its underground network as a general guide only on the strict understanding that it is based on the best available information provided by each Local Authority in Ireland to Irish Water. Irish Water can assume no responsibility for and give no guarantees, undertakings or warranties concerning the accuracy, completeness or up to date nature of the information provided and does not accept any liability whatsoever arising from any errors or omissions. This information should not be relied upon in the event of excavations or any other works being carried out in the vicinity of the Irish Water underground network. The onus is on the parties carrying out excavations or any other works to ensure the exact location of the Irish Water underground network is identified prior to excavations or any other works being carried out. Service connection pipes are not generally shown but their presence should be anticipated.

#### **General Notes:**

- 1) The initial assessment referred to above is carried out taking into account water demand and wastewater discharge volumes and infrastructure details on the date of the assessment. The availability of capacity may change at any date after this assessment.
- 2) This feedback does not constitute a contract in whole or in part to provide a connection to any Irish Water infrastructure. All feasibility assessments are subject to the constraints of the Irish Water Capital Investment Plan.

- 3) The feedback provided is subject to a Connection Agreement/contract being signed at a later date.
- 4) A Connection Agreement will be required to commencing the connection works associated with the enquiry this can be applied for at <a href="https://www.water.ie/connections/get-connected/">https://www.water.ie/connections/get-connected/</a>
- 5) A Connection Agreement cannot be issued until all statutory approvals are successfully in place.
- 6) Irish Water Connection Policy/ Charges can be found at https://www.water.ie/connections/information/connection-charges/
- 7) Please note the Confirmation of Feasibility does not extend to your fire flow requirements.
- 8) Irish Water is not responsible for the management or disposal of storm water or ground waters. You are advised to contact the relevant Local Authority to discuss the management or disposal of proposed storm water or ground water discharges
- 9) To access Irish Water Maps email <a href="mailto:datarequests@water.ie">datarequests@water.ie</a>
- 10) All works to the Irish Water infrastructure, including works in the Public Space, shall have to be carried out by Irish Water.

If you have any further questions, please contact Kevin McManmon from the design team at kmcmanmon@water.ie For further information, visit www.water.ie/connections.

Yours sincerely,

Yvonne Harris

Gronne Haceis

**Head of Customer Operations** 

C. Irish water Statement of Design Acceptance



Laura Ruiz Garrido
Block S
Eastpoint Business Park
Alfie Byrne Road
D03H3F4
Dublin
Ireland

30 June 2022

Uisce Éireann Bosca OF 448 Oifig Sheachadta na Cathrach Theas Cathair Chorcal

Irish Water PD Box 448, South City Delivery Office, Cark City.

www.water.ie

Re: Design Submission for Ravens Rock Road, Sandyford, Dublin (the "Development") (the "Design Submission") / Connection Reference No: CDS21008079

Dear Laura Ruiz Garrido,

Many thanks for your recent Design Submission.

We have reviewed your proposal for the connection(s) at the Development. Based on the information provided, which included the documents outlined in Appendix A to this letter, Irish Water has no objection to your proposals.

This letter does not constitute an offer, in whole or in part, to provide a connection to any Irish Water infrastructure. Before you can connect to our network you must sign a connection agreement with Irish Water. This can be applied for by completing the connection application form at <a href="https://www.water.ie/connections">www.water.ie/connections</a>. Irish Water's current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities (CRU)(<a href="https://www.cru.ie/document\_group/irish-waters-water-charges-plan-2018/">https://www.cru.ie/document\_group/irish-waters-water-charges-plan-2018/</a>).

You the Customer (including any designers/contractors or other related parties appointed by you) is entirely responsible for the design and construction of all water and/or wastewater infrastructure within the Development which is necessary to facilitate connection(s) from the boundary of the Development to Irish Water's network(s) (the "Self-Lay Works"), as reflected in your Design Submission. Acceptance of the Design Submission by Irish Water does not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.

If you have any further questions, please contact your Irish Water representative:

Name: Antonio Garzón

Email: antonio.garzon@water.ie

Yours sincerely,

vonne Haccis

**Yvonne Harris** 

**Head of Customer Operations** 

## Appendix A

#### **Document Title & Revision**

- 21-118-P221 Proposed Foul Water Drainage Layout at 00 Lower Ground Level
- 21-118-P250 Proposed Water Supply Layout

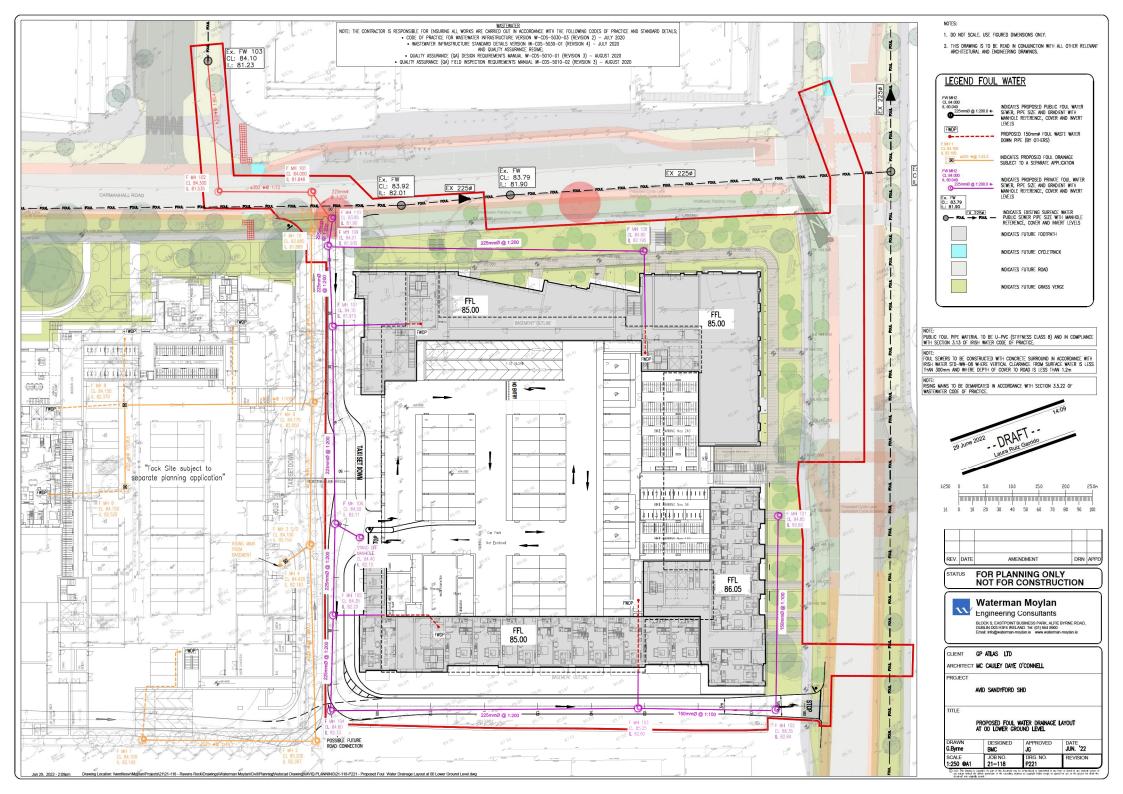
#### **Additional Comments**

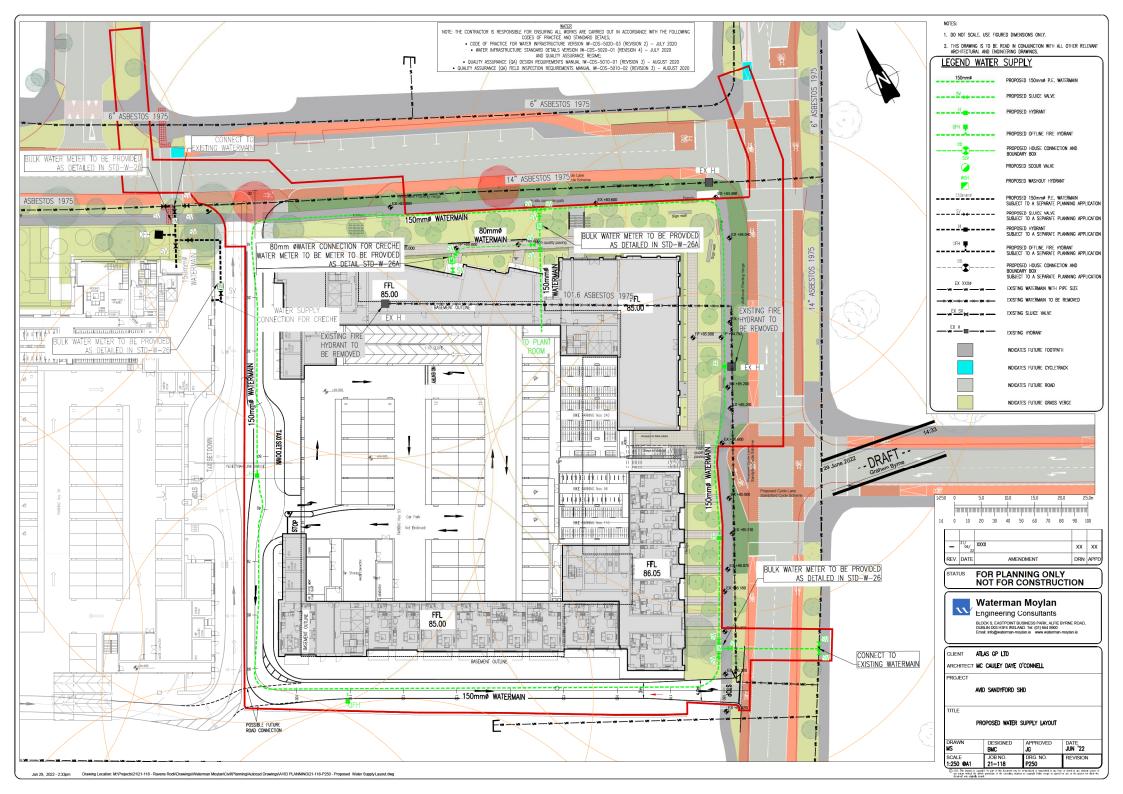
The design submission will be subject to further technical review at connection application stage.

This Statement of Design Acceptance is valid for the development over the SHD Avid Site (east side). Previously TACK SHD SODA was issued in April.

For further information, visit www.water.ie/connections

Notwithstanding any matters listed above, the Customer (including any appointed designers/contractors, etc.) is entirely responsible for the design and construction of the Self-Lay Works. Acceptance of the Design Submission by Irish Water will not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.





# D. Site Investigation Avid Site

PROPOSED DEVELOPMENT SANDYFORD DUBLIN MARLET PROPERTY

AECOM CONSULTING ENGINEERS

# CONTENTS

I INTRODUCTION
II FIELDWORK
III TESTING
IV DISCUSSION

# APPENDICES

1	BORING RECORDS
H	ROTARY CORE LOGS / PHOTOGRAPHS
III	TRIAL PIT RECORDS
IV	PLATE BEARING TEST
V	RDE DICEST 265 INFILTDATION

V BRE DIGEST 365 INFILTRATION VI TEST DATA

a. Geotechnical

b. Environmental / Chemicalc. Ground Water and Gas

VII SITE PLAN

#### **FOREWORD**

The following Conditions and Notes on Site Investigation Procedures should be read in conjunction with this report.

#### General.

Recommendations made, and opinions expressed in the report are based on the strata observed in the exploratory holes, together with the results of in-situ and laboratory tests. No responsibility can be held for conditions which have not been revealed by exploratory work, or which occur between exploratory hole locations. Whilst the report may suggest the likely configuration of strata, both between exploratory hole locations, or below the maximum depth of the investigation, this is only indicative, and liability cannot be accepted for its accuracy.

Unless specifically stated, no account has been taken of possible subsidence due to mineral extraction below or close to the site.

# Boring Procedures.

Unless otherwise stated, the 'Shell and Auger' technique of soft ground boring has been employed. All boring operations sampling and/or logging of soils and in-situ testing complies with the recommendations of the British Standard Code of Practice BS 5930 (1981), 'Site Investigation' and BS 1377:1990, 'Methods of test for soils for civil engineering purposes'.

Whilst the technique allows the maximum data to be obtained in soft ground, some disturbance and variation of soft and layered soils is unavoidable. Attention is drawn to this condition, whenever it is suspected. Where cobbles and boulders are recorded, no conclusion should be drawn concerning the size, presence, lithological nature, or numbers per unit volume of ground.

Where peat has been encountered during siteworks, samples have been logged in accordance with the Von Post Classification (ref. Von Post, L. 1992. Sveriges Gologiska Undersoknings torvinventering och nogra av dess hittils vunna resultat (SGU peat inventory and some preliminary results) Svenska Mosskulturforeningens Tidskrift, Jonkoping, Swedden, 36, 1-37 & Hobbs N. B. Mire morphology and the properties of some British and foreign peats. QJEG, Vol. 19, 1986).

# Routine Sampling.

Undisturbed samples of soils, predominantly cohesive in nature are obtained unless otherwise stated by a 104mm diameter open-drive tube sampler. In granular soils, and where undisturbed sampling is inappropriate, disturbed samples are collected. Smaller disturbed samples are also recovered at intervals to allow a visual examination of the full strata section.

# In-Situ Testing.

Standard penetration tests, utilising either the standard split spoon sampler or solid cone and automatic trip-hammer are conducted unless otherwise where required by instruction. Subsequent to a seating drive of 150mm, a summation for the number of blows for 300mm penetration is recorded on the boring records together with the blow count for each 75mm penetration. In cases where incomplete penetration is obtained, the number of blows for the recorded value of penetration are noted. In coarse granular soils, a cone end is fitted to the sampler and a similar procedure adopted.

#### Groundwater.

The depth of entry of any influx of groundwater is recorded during the course of boring operations. However, the normal rate of boring does not usually permit the recording of an equilibrium level for any one water strike. Where possible drilling is suspended for a period of twenty minutes to monitor the subsequent rise in water level.

Groundwater conditions observed in the borings or pits are those appertaining to the period of investigation. It should be noted however, that groundwater levels are subject to diurnal, seasonal and climatic variations and can also be affected by drainage condition, tidal variation or other causes.

# Retention of Samples.

After satisfactory completion of all the scheduled laboratory tests on any sample, the remaining material is discarded unless a period of retention of samples is agreed, it is our normal practice to discard all soil samples one month after submission of our final report.

# REPORT ON A SITE INVESTIGATION AT FORMER AVID SITE

# SANDYFORD FOR

# MARLET PROPERTY GROUP AECOM CONSULTING ENGINEERS

Report No. 22455

**JUNE 2020** 

## I Introduction

A new multi-storey residential development is proposed for this site located at the junction of Blackthorn Road and Carmanhall Road in Sandyford. The site was formerly occupied by AVID, the old buildings have all been demolished and the area prepared for this new development.

An investigation of sub soil conditions in the developments area has been carried out by IGSL under the direction of AECOM Consulting Engineers, acting for the developers, MARLET Property Group.

The scope of works scheduled and completed is detailed below:

*	Cable Percussion Boreholes	4 nr.
•	Rotary Core Drilling	2 nr.
•	Trial Pits	12 nr.
•	CBR by Plate Test	1 nr.
•	Infiltration Test	2 nr.
	Water and Gas Manitorina	

- Water and Gas Monitoring
- Geotechnical Laboratory Tests
- **Environmental Laboratory Tests**

The investigation has been carried out in accordance with the various standards outlined in the foreword to this document. Field operations were completed in March 2020.

This report includes all factual data from field operations and laboratory including detailed geotechnical logs and laboratory data.

Recommendations for foundation construction are also presented in this report.

#### II Fieldwork

The development area is Brownfield following demolition of buildings and site preparation works. The surfaces ranged from hard-core fill to tarmac and topsoil.

The various exploratory locations are noted on the drawing enclosed in Appendix VII. This drawing was provided by AECOM. Each location was set out to the specified coordinates by IGSL site personnel.

All exploratory positions were scanned electronically (CAT) to ensure that existing services were not damaged. Hand excavation was also carried out to a depth of 1.00 metres at borehole locations to ensure that underground services were not damaged.

The various exploratory methods are discussed in the following paragraphs.

#### Boreholes

Boreholes were 200mm diameter and were constructed using conventional cable percussion equipment. Holes were referenced BH01 to BH04 and were located at the four corners of the site

Detailed geotechnical records are contained in Appendix I to this report - the records give details of stratification, sampling, in-situ testing and groundwater. Note is also taken of any obstructions to normal boring requiring the use of the heavy chisel for advancement. It was not possible to recover undisturbed samples because of the high stone/cobble content of the strata encountered.

The findings at the four locations are quite consistent. Surface FILL extends to depths ranging from 1.00 to 1.90 metres.

In all four boreholes stiff to very stiff brown and grey sandy gravelly CLAY is present below the FILL Boreholes continued in this stratum to refusal on obstructions at depths ranging from 7.30 to 11.20 metres. An increasing strength with penetration depth has been noted. Cobbles and boulders were present in the gravelly clay stratum.

This gravelly clay is GLACIAL TILL or BOULDER CLAY, very typical of the greater Dublin area.

BH02 and BH04 were dry during boring while slow to moderate water seepages were noted at 3.30 metres in BH01 and 3.10 metres in BH03. Slotted standpipes were installed in BH01 and BH02 to facilitate long term observation of ground water and permit measurement of any gas present.

# Rotary Core Drilling

Rotary core drilling was scheduled at two locations to advance hole depth and establish bedrock horizon. These holes were bored through the boulder clay deposits to the underlying granite bedrock. Rotary holes were designated RC02 and RC04.

A GEO405 rig was used to drill and recover 78mm diameter core of rock using triple tube diamond drilling technique. Open-hole Symmetrix Drilling was used in the overburden soils

All recovered core was returned to the laboratory for detailed logging and photography. The geotechnical core logs are contained in Appendix II. The logs note Total Core Recovery (TCR), Solid Core Recovery (SCR), Rock Quality Designation (RQD) as well as presenting a fracture spacing log and detailed geological description.

The drilling was advanced through overburden described as stiff brown and black very gravelly clay with cobbles and boulders throughout.

Weak to Medium Strong grey GRANITE was noted in RC02 at 8.70 metres BGL and 100% core was recovered from 8.70 to 11.70 metres. This core was quite fractured with low SCR and RQD values.

At RC04 very weathered GRANITE was noted at 11.10 metres BGL. Drilling continued to 14.80 metres with only limited recovery of solid core in this location.

Sub samples of the recovered core were taken and sent to the materials laboratory for Point Load Strength Tests.

A 50mm slotted PVC standpipe was installed in both locations with gravel surround and surface seal, details of the installations are provided on the drilling record. Water was noted at final standing levels of 2.20 and 1.32 metres BGL.

#### Trial Pits

Trial Pits were excavated at twelve locations to establish stratification and permit sample recovery for environmental analysis. Trial Pits are referenced TP01 to TP12 and fully detailed records are presented in Appendix III. Photographs were also taken at each trial pit and these are also attached for record purposes.

The pits reflect a very high degree of consistency with FILL in all locations (varying from 0.30 to 1.20 metres in thickness) overlying stiff to very stiff BOULDER CLAY. All trial pits were completed at 3.00 metres and no ground water was encountered during the course of the investigation, other than a minor seepage at 2.00 metres in TP01. Excavations remained stable throughout.

Trial Pits were backfilled with compacted excavated material and the areas levelled.

# Plate Bearing Test

The CBR value of the soil at shallow depth was established at one locations using Plate Bearing Test Apparatus. A steel plate is loaded and off-loaded incrementally over two stages and the deflection under load and recovery under off-load is measured by a system of dial gauges. The data is processed and load settlement graphs are prepared. An equivalent CBR value is calculated in accordance with NRA HD25-26/10.

The test was carried out at 0.50 metres on MADE GROUND. An equivalent CBR value of 10% was obtained on the Load Cycle, increasing considerably on re-load.

Test data sheets are presented in Appendix IV.

# Infiltration Tests

Two infiltration tests were carried out in accordance with BRE Digest 365 in the specified locations. Test data is presented in Appendix V.

In both locations no fall in water table was noted over the specified period and a ZERO Infiltration Rate was recorded. The results are typical of the very low permeability boulder clays present on the site and in the general area.

The use of the local authority drainage system for disposal of storm and surface water is therefore recommended.

# Water and Gas Monitoring

Standpipes were installed in four locations to facilitate long term monitoring of ground water levels and determine gas concentrations. Measurements were carried out at intervals following site completion.

Details are presented in Appendix VIc. Final standing water level has stabilised at approximately 2.00 metres BGL.

Concentrations of CO2, O2, and CH4 are negligible and no safety issues arise in this regard.

# III. Testing

#### a) In-Situ:

Standard penetration tests were carried out at approximate 1.00 metre intervals in the geotechnical boreholes to measure relative in-situ soil strength. Tests were also carried out in the rotary holes. N values are noted in the right hand column of the individual records, representing the blow count required to drive the standard sampler 300mm into the soil, following initial seating blows. Where full test penetration was not achieved the blow count for a specific penetration is recorded, or refusal is indicated where appropriate. Results are summarised as follows.

Stratum / Depth	N Value Range	Comment
FILL DEPOSITS	14 to 17	Medium Dense
BOULDER CLAY		
2.00 metres BGL	21 to 32	Stiff
3.00 metres BGL	18 to 32	Stiff
1.00 metres BGL	28 to 43	Stiff to Very Stiff
5.00 metres BGL	35 to 42	Very Stiff
5.00 metres BGL	36 to 43	Very Stiff
7.00 metres BGL	39 to +50	Very Stiff to Hard
3.00 to 10.00	40 to +50	Very Stiff to Hard

Refusal of SPT apparatus was recorded at the base of each borehole possibly indicative of the granite bedrock horizon.

### (b) Laboratory:

A programme of laboratory testing was scheduled following completion of site operations. Geotechnical soil and rock testing was carried out by IGSL in its INAB-Accredited laboratory. Chemical testing was performed by CHEMTEST in a UKAS accredited laboratory.

The overall test programme included the following elements:

*	Moisture Content	IGSL
•	Liquid and Plastic Limits	IGSL
•	PSD Grading by wet sieve	IGSL
•	PSD Grading by Hydrometer	IGSL
•	Point Load Test on Rock Core	IGSL
•	Sulphate Chloride and pH	CHEMTEST
•	RILTA Suite Environmental	CHEMTEST

All test data is presented in Appendices VIa and VIb. and individual test results are discussed as follows:

# Classification / Moisture Content

Six samples of the gravelly CLAY stratum from the boreholes had index properties established. Results consistently fall into Zone CL of the standard Classification, indicative of low plasticity sensitive clay matrix soils. Moisture content for the samples ranges from 11% to 17%. Results are typical of the local boulder clay.

### Grading

Wet sieve analysis and hydrometer was used to establish PSD grading curves for four samples of the glacial till. The graphs reflect material graded smoothly from the clay to gravel fraction, the straight-line pattern of the graphs is typical of the local boulder clay deposition.

#### Point Load Test

The strength of the limestone bedrock has been established by Diametric Point Load Tests on four segments of core. Equivalent UCS values ranging from 4 to 40 MPa with an average UCS value of 23 MPa. The low results reflect the highly weathered and weak nature of the bedrock.

#### Chemical (BRE SOI Suite)

Five soil samples were selected for sulphate, Chloride and pH analysis. Sulphate concentrations (SO4 2:1 extract) of < 0.010 g/l were established with pH values of 8.4 to 8.7. Chloride contents were also consistently low <0.010 g/l. A sulphate design class of DS-1 (ACEC Classification for Concrete) is indicated for sulphate concentrations less than 0.5 g/l. No special precautions are therefore required to protect foundation concrete from sulphate or chloride aggression.

#### RILTA Suite Environmental

Sixteen samples of the MADE GROUND taken at 0.50 to 1.00 metre from each trial pit were submitted for detailed analysis to RILTA Suite (WAC) parameters.

Fifteen of the sixteen samples are classified as INERT with no elevated contaminant levels established.

In one sample however (TP05 @ 0.50m BGL) an elevated sulphate content was recorded, in excess of the permitted INERT limit. The remaining levels recorded in this sample were all below the INERT levels.

No traces of Asbestos were noted during routine screening.

#### IV Discussion:

A new multi-storey residential development is to be undertaken on this site in Sandyford. The nine-storey building will incorporate a single storey basement car park. A formation depth some 3.50 to 4.00 metres BGL is envisaged.

A detailed investigation of sub soil and bedrock conditions has been carried out under the direction of AECOM Consulting Engineers on behalf of MARLET Property Group.

# Summary Stratification

The findings are very consistent and confirm the presence of shallow surface FILL over BOULDER CLAY deposits with GRANITE bedrock encountered at depth between approximately 9.00 and 11.00 metres.

The FILL extends to a maximum depth of about 1.50 metres and is firm or medium dense in situ, with N values in the range 14 to 17 and an in situ CBR value of 10%.

The BOULDER CLAY or glacial till comprises stiff to hard brown, grey and black sandy gravelly CLAY typically containing cobbles and boulders. SPT values increase with depth from about N=20 at 2.00 metres BGL to N > 50 below 7.00 metres.

The characteristics of the Dublin boulder clay are very well documented and the laboratory data for this site is consistent with the published data.

Ground water seepages were noted in several locations and long term water observations in standpipes indicates a final standing level of about 1.50 metres BGL for this site.

Variation in the general grading pattern of the till can occur, with an elevated granular content and increased moisture content often identified. Bands of water bearing clayey gravel can also typically occur within the generally cohesive soils.

#### Proposed Development

With regard to the proposed development (incorporating multi-storey construction over basement) the following geotechnical issues are discussed.

- Foundations / Bearing Capacity
- Piling
- Basement Construction
- Excavation / Ground Retention
- Groundwater Control / Uplift

# Foundations / Bearing Capacity

At an assumed basement formation depth of 4.00 metres BGL, the sub soils consist of very stiff to hard dark brown or grey gravelly CLAY (Boulder Clay). SPT values at this depth range from N=28 to N=43 with an average value of N=36.

The boulder clay at 4.00 metres BGL should readily support an allowable bearing pressure of the order of 325 KPa for basement slab or column base construction.

N values at 5.00 metre BGL show an increase, with an allowable bearing pressure of the order of 375 KPa recommended at this depth.

The characteristics of the local boulder clay are well documented with numerous publications detailing behavioural and strength / settlement characteristics. The field and laboratory findings from this site are consistent with the extensive local data. The boulder clay will be sensitive to moisture content variation and should be protected from rainfall by blinding. Visual inspection of excavated formation by experienced personnel is also recommended to ensure uniformity and suitability of the founding medium. Any soft zones encountered should be removed and replaced with low-grade concrete.

Settlement in the very stiff to hard glacial till under the above loads should not exceed 5mm and differential movement should be negligible.

# Piling

Should direct excavation to a suitable bearing stratum prove uneconomic from either an engineering or environmental viewpoint, the use of piling techniques can be considered.

Various piling techniques are available with specialist contractors, experienced in local ground conditions available to provide this service.

The stiff to hard black till encountered at about 2.00 metres extends to bedrock horizon at about 10.00 metres and can be used as founding medium for light to moderately loaded piles.

For multi-storey structures with high column loads it is likely that large diameter piles, rock socketed into the granite bedrock will be required.

Proof core drilling has indicated the presence of highly weathered non-intact granite at the soil rock interface, in excess of 3.00 metres in places.

Piling contractors should be consulted to determine the optimum solution for this site, having regard to the geotechnical data and to any possible environmental restraints.

#### **Basement Construction**

As a basement will be incorporated over the full footprint the very stiff to hard lodgement till at approximately 3.50 to 4.00 metres BGL is recommended as founding medium with an allowable bearing pressure of 300 to 350 KPa indicated by SPT values averaging N=36.

Settlement under this intensity of load will be low (< 5mm) and differential settlement will be negligible.

#### Excavation / Ground Retention

Assuming 4.00 metre deep basement construction a retaining wall structure will probably be required to support the soils, prevent undermining of sensitive adjoining buildings or roadways and preclude ground water ingress.

A number of ground retention techniques are available and each should be fully evaluated. These include the following:

- Steel Sheet Pile Wall
- Secant Pile Wall
- King Post Wall

Specialist contractors with will advise on the most suitable and economic option for this development.

#### Groundwater

Water ingress was noted in two of the boreholes at approximately 3.00 metres. The inflow was slight to moderate and control of ground water in basement excavation should be readily achieved by conventional pumping from local sumps.

Long-term water observation in standpipes has indicated a final standing level at approximately 2.00 metres BGL and this figure should be adopted in design against uplift.

# Roads / Car Parking

A CBR value of 10% was obtained at 0.50 metres BG in the upper medium dense FILL. This should be suitable for pavement design. Visual inspection of pavement formation is recommended to ensure that all suspect or organic material is removed prior to construction.

# Infiltration

Two percolation tests to BRE Digest 365 confirmed that the soils are unsuitable for dispersion of storm and surface water. The Local Authority drainage system should be utilised.

#### Environmental

The results of WAC analyses showed that one sample failed to satisfy the criteria for Inert waste as stipulated by the European Landfill Directive. The fact that only one element of one test out of sixteen analysed exceeded the INERT level, suggests that consultation with landfill operators may well result in acceptance of excavated material from this site.

The results of the RILTA Suite tests can be used to carry out a full Waste Characterisation Assessment (WCA). This assessment is carried out by an environmental specialist and determines whether the soils are Hazardous or Non-Hazardous in advance of being despatched to landfill. Given the test results a WCA may be relevant to this site and may be required by the landfill operators in the event of major excavation.

#### Concrete

Low sulphate and chloride contents were established with near neutral pH values. No special precautions are deemed necessary to protect foundation concrete.

<u>IGSL/JC</u> June 2020





BH LOG

# GEOTECHNICAL BORING RECORD

REPORT NUMBER

22455

BOREHOLE NO. CONTRACT BH1 Avid Site, Sandyford SHEET Sheet 1 of 1 RIG TYPE **CO-ORDINATES** Dando 2000 DATE COMMENCED 24/03/2020 BOREHOLE DIAMETER (mm) 200 GROUND LEVEL (m AOD) DATE COMPLETED 25/03/2020 BOREHOLE DEPTH (m) 7.30 CLIENT SPT HAMMER REF. NO. **BORED BY** Marlet W.Cahill **ENGINEER AECOM ENERGY RATIO (%)** PROCESSED BY I.Reder Samples Standpipe Details E Depth (m) Elevation Sample Type Recovery Legend Field Test Depth Description Depth (m) Results -0 1. 11/ TOPSOIL 0.20 MADE GROUND (comprised of angular broken rock 0.60 MADE GROUND (Comprised of gravelly clay with 1.00 some stone) AA135559 B 1.00 Firm to stiff, dark brown, sandy silty CLAY with some N = 17 (6, 7, 4, 4, 4, 5) gravel and occasional cobbles -2 AA135560 B 2.00 (4, 4, 5, 5, 5, 6) 2.50 Stiff, dark grey, sandy silty gravelly CLAY with occasional cobbles 3 4 5 6 7 AA135561 8 3.00 (4, 5, 6, 6, 7, 7) AA135562 8 4.00 4.30 N = 33 (6, 7, 7, 8, 8, 10) Very stiff, brown, sandy gravelly silty CLAY with many **®** subangular to subrounded cobbles and boulders AA135563 B 5.00 N = 35 (4, 6, 7, 8, 8, 12) AA135564 8 6.00 N = 40 (7, 8, 8, 9, 11, 12) AA135565 В 7.00 N = 50/40 mm 7.30 (25, 50) Obstruction End of Borehole at 7.30 m - 9 HARD STRATA BORING/CHISELLING WATER STRIKE DETAILS Time Water Casing Sealed Rise Time From (m) To (m) Comments Comments Strike Depth To (h) At (min) 4.8 5.1 7.3 0.75 Moderate 3.80 3.80 5.00 1.70 20 29/5/20 7.2 2 GPJ IGSL.GDT **GROUNDWATER PROGRESS** Hole Casing Depth to Water **INSTALLATION DETAILS** Date Comments Depth Depth Date Tip Depth RZ Top RZ Base Type 25-03-20 7.30 1.00 7.00 50mm SP REMARKS Hand dug inspection pit for services Sample Legend D - Small Disturbed (tub) 8 - Bulk Disturbed LB - Large Bulk Disturbed Env - Environmental Sample (Jar + Vial + Tub) Sample P - Undisturbed Piston Sample W - Water Sample



# **GEOTECHNICAL BORING RECORD**

REPORT NUMBER

22455

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							egend Elevation Depth (m)					San	ples				0
				Descrip	ption		Legend				Ref. Number	Sample Type	Depth	(E)	Recovery	Field Test Results	Standpipe
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2	Stiff to with c	o very sti cobbles	iff , dark	grey, s	sandy gra	velly silty CLA	Y	x(			SPL2	9	2.0			N = 23 (4, 5, 5, 5, 6, 7)	0 0
3	Very	stiff, light	brown.	very s	andy CLA	Y with some	\(\frac{\infty}{2}\)			3.80	SPL3	В	3.0			N = 32 (5, 7, 7, 8, 8, 9)	0 0 0
	grave							0			SPL4	В	4.0			N = 43 (6, 8, 10, 10, 11, 12)	0 0 0
	Very s	stiff to ha	ard , grey	and g	grey/brow y subang	n, sandy	- 0			5.40	SPL5	В	5.0	0		N = 42 (9, 10, 10, 10, 11, 11)	0
	subro	unded c	obbles a	nd bo	y subang ulders	uidi (O					SPL6	В	6.0	0		N = 44 (8, 9, 9, 10, 11, 14)	0 0
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		uction of Boreho	ole at 8.5	0 m	***************************************		Ø.	4 6		8.50	SPL8	8	8.20	0		N = 50/75 mm (12, 16, 32, 18)	0
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### GEOTECHNICAL BORING RECORD

REPORT NUMBER

22455

BOREHOLE NO. **BH3** CONTRACT Avid Site, Sandyford SHEET Sheet 1 of 1 **RIG TYPE** Dando 2000 **CO-ORDINATES** DATE COMMENCED 23/03/2020 BOREHOLE DIAMETER (mm) 200 DATE COMPLETED 24/03/2020 GROUND LEVEL (m AOD) BOREHOLE DEPTH (m) 8.30 CLIENT SPT HAMMER REF. NO. BORED BY W.Cahill Marlet ENGINEER PROCESSED BY I.Reder **AECOM ENERGY RATIO (%)** Samples Standpipe Details Ξ E Elevation Sample Recovery Ref. Number Field Test Depth ( Depth egend Description Depth (m) Results - 0 TARMAC 0.15 MADE GROUND (comprised of angular gravel -0.30 C.L.804) MADE GROUND (Comprised of brown sandy gravelly clay fill with some brick and concrete fragments) AA135551 1.00 В 1.20 (2, 2, 3, 3, 4, 4) Stiff grey/brown sandy silty CLAY with some gravel and occasional cobbles N = 20 (3, 4, 4, 5, 6, 5) -2 AA135552 B 2.00 N = 18 (3, 4, 5, 5, 4, 4) AA135553 B 3.00 3.90 N = 50/210 mm Very stiff dark brown gravelly CLAY AA135554 B 4.00 (6, 14, 14, 20, 16) N = 35 (5, 6, 8, 8, 9, 10) AA135555 B 5.00 -0 - Q N = 36 (6, 7, 7, 8, 10, 11) -6 AA135556 В 6.00 6.40 Very stiff, brown and grey/brown, sandy gravelly silty CLAY with many subangular to subrounded cobbles Ø0 and boulders AA135557 N = 40 (7, 8, 10, 10, 9, 11) B 7.00 N = 50/75 mm (10, 14, 46, 4) AA135558 B 8.00 8.30 Obstruction End of Borehole at 8.30 m - 9 HARD STRATA BORING/CHISELLING WATER STRIKE DETAILS Water Time Casing Sealed Rise Time From (m) To (m) Comments Comments (h) Strike Depth At To (min) 4.2 4.5 3.10 3.10 4.20 1.60 20 Moderate IGSL.GDT 29/5/20 8.3 2 8 GROUNDWATER PROGRESS Hole Casing Depth to Water INSTALLATION DETAILS Date Comments Depth Depth Date | Tip Depth RZ Top | RZ Base Type REMARKS Hand dug inspection pit for services Sample Legend D - Small Disturbed (tub) B - Bulk Disturbed LB - Large Bulk Disturbed Sample P - Undisturbed Piston Sample onmental Sample (Jar + Vial + Tub) W - Water Sample



29/5/20

22455.GPJ

BHLOG

### GEOTECHNICAL BORING RECORD

REPORT NUMBER

22455

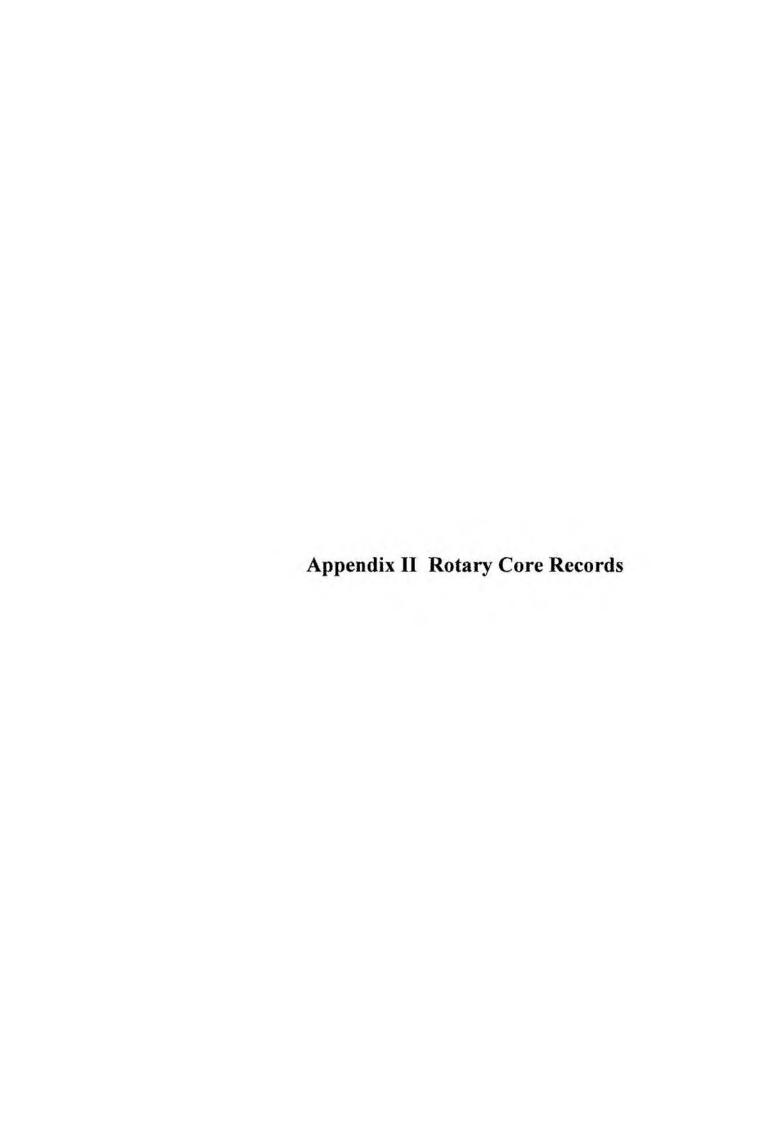
BOREHOLE NO. CONTRACT **BH4** Avid Site, Sandyford SHEET Sheet 1 of 2 **RIG TYPE** Dando 2000 CO-ORDINATES DATE COMMENCED 20/03/2020 BOREHOLE DIAMETER (mm) 200 DATE COMPLETED 23/03/2020 GROUND LEVEL (m AOD) BOREHOLE DEPTH (m) 11.20 CLIENT SPT HAMMER REF. NO. BORED BY W.Cahill Marlet **ENERGY RATIO (%)** ENGINEER PROCESSED BY **AECOM** I.Reder Samples Standpipe Details E E Sample Type Elevation Recovery Ref. Number Field Test Legend Depth ( Depth Description Depth (m) Results - 0 TARMAC 0.15 MADE GROUND (comprised of angular gravel -0.30 C.L.804) Firm to stiff, dark brown, sandy silty CLAY with some gravel (Possibly Made Ground) 0.00 0.00 0.00 0.00 0.00 AA130581 1.00 N = 17 В (2. 3, 4, 4, 4, 5) O 2 1.80 Q Very stiff, dark brown/black, sandy silty gravelly CLAY XO \_\_\_\_ N = 32 (5, 6, 8, 8, 7, 9) AA130582 8 2.00 \_\_\_\_ -X-- X-N = 24 (3, 4, 4, 5, 7, 7) 3.10 AA130583 8 3.00 Stiff, dark brown, very sandy gravelly CLAY with some (9. <u>~</u>0 0. 0 N = 28(4, 5, 6, 7, 7, 8) AA130584 8 4.00 4.20 Stiff to very stiff, brown and brown/grey, sandy Ø⋻ gravelly silty CLAY with many cobbles and occasional 0x boulders AA130585 B 5.00 5 (6, 8, 8, 9, 9, 9) N = 43 (6, 8, 10, 10, 11, 12) AA130586 8 6.00 AA130587 7.00 N = 42 (7, 9, 9, 10, 12, 11) N = 41 (6, 7, 9, 11, 10, 11) AA130158 B 8.00 AA130589 8 9.00 9 (7, 9, 10, 11, 10, 12) HARD STRATA BORING/CHISELLING WATER STRIKE DETAILS Rise Time Water Casing Sealed Time To (m) Comments From (m) Comments (h) Strike Depth (min) 2.3 2.5 1.25 No water strike 6.7 0.75 6.4 11.2 10.9 2 IGSL, GDT GROUNDWATER PROGRESS Hole Casing Depth to Water INSTALLATION DETAILS Comments Date Depth Depth Tip Depth RZ Top RZ Base 20-03-20 23-03-20 Type DRY 1.70 REMARKS Hand dug inspection pit for services Sample Legend
D - Small Disturbed (lub)
B - Bulk Disturbed
LB - Large Bulk Disturbed UT - Undisturbed 100mm Diameter Sample P - Undisturbed Piston Sample GSL ironmental Sample (Jar + Vial + Tub)

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#### GEOTECHNICAL BORING RECORD

REPORT NUMBER

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GRO	DUND	LEVEL (	m AOD)				OLE DEPTH			1.20	1	DATE COMPLETED 23/03/2020					
	INEE		arlet ECOM				MMER REF. Y RATIO (%)				PROCES	W.Cahill BY I.Reder					
E								5	(E)	-		ples	1 2	2 = 117	ed		
Depth (m)			D	escription			Legend	Elevation	Depth (m)	Ref. Number	Sample Type	Depth (m)	Recovery		Standpipe		
10	grave	to very st elly silty C ders (con	CLAY with	and brown/ many cobb	grey, sandy les and occa	isional			11.20	AA130590		10.00		N = 48 (8, 8, 10, 10, 12, 14) N = 50/95 mm (13, 12, 27, 23)			
12	Obst End	ruction of Boreho	ole at 11.2	0 m						The second secon			and the second s	(13, 12, 27, 23)			
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2. 6. 10	3 4 .9	To (m) 2.5 6.7 11.2	Time (h) 1.25 0.75 2			B.		De			То	(n	me nin)	Comments  No water strike  ROUNDWATER PRO			





# GEOTECHNICAL CORE LOG RECORD

REPORT NUMBER

22455

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ONTRA	ACT	A	vid Sit	e, Sand	lyford							DRILL	HOLE T	NO	RC	02 et 1 of 2	2
O-ORE			(mOD)	)				RIG TYPE FLUSH	DATE	DATE COMMENCE DATE COMPLETE			3/2020				
IENT	ER		arlet ECOM		γ			INCLINATION	FLUSH Air/Mist INCLINATION (deg) -90 CORE DIAMETER (mm) 78						IGSL D.O'Shea		
Core Run Depth (m)	T.C.R.%	S.C.R.%	R.Q.D.%		cing og m)	Non-intact Zone	Legend		Description							Standpipe Details	SPT (N Value)
								SYMMETRIX DRILLING: No recovery, observed by driller as returns of MADE GROUND consisting of clayey gravel  SYMMETRIX DRILLING: No recovery, observed by driller as returns of grey brown black silbs sandy gravelly CLAY									
							0 0		as returns of grey brown black silty sandy gravelly CLAY								
							000	SYMMETRIX as returns of g SYMMETRIX	grey bro	wn clayey	sandy GRA	VEL		2.30			
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8.70							+++++++	SYMMETRIX as returns of p	DRILLI	NG: No rec e weathere	covery, obse d ROCK	erved by dr		8.70			
9.30	100	100	85				+++++++		-0-01-01-0								
MAR	KS			·			++							WAT	ERS		DETAILS
le ca	sed C	.00-8	3.70m						/ater trike	Casing Depth	Sealed At	Rise To	Time (min)		mmer		
														N	o wate	er strike	recorde
			=		unanemiero de la compensa de la comp	-				1			7			WATER	DETAIL
			ETAIL		1020				Date	Hole Depth	Casing Depth	Depth to Water	Com	ments	3		
Date 2-03-2		11.7		8.10	RZ Base 11.70		50m	m SP									



# **GEOTECHNICAL CORE LOG RECORD**

REPORT NUMBER

22455

	NTR			וט טו	te, Sandyford							SHE	LHOLE ET		RC	et 2 of	2		
		D LE	ES VEL (I	mOD	)			RIG TYPE FLUSH	E Ge0405				DATE COMMENCED 11/03/2020 DATE COMPLETED 12/03/2020						
	ENT			arlet CON	1			INCLINATI	100	DRILLED BY IGSL LOGGED BY D.O'Shea									
Downhole Depth (m)	Core Run Depth (m)	T.C.R.%	S.C.R.%	R.O.D.%	Fracture Spacing Log (mm)	Non-intact Zone	Legend			Descrip	ition			Depth (m)	Elevation	Standpipe Details	SPT (N Value)		
0	10.70	100	0	0			++++++	weak, ma grey/black	ssive to str white mo	re compete ructureless, ttled, fine to	rained.								
*						E	+++	(contribut	GRANITE, slightly to predominantely highly weathered (contributing to coreloss at 9.30-10.70m, 11.32-11.38m & 11.46-11.70m).  Discontinuities are rough, irregular. Apertures are open, commonly sandy clay-smeared. Dips are irregular.							•			
	11.70	100	25	19	=		+++++++++++++++++++++++++++++++++++++++												
2 3 4	The state of the s							\(continuec	d)	e at 11.70 r		едиа.		111.70					
-	MARIA e cas		00-8.	70m					Water Strike	Casing Depth	Sealed At	Rise To	Time (min)	7	ER ST		DETAIL		
					Ä				Suite	DEDUI	AL.	10	(111(1)			9200	record		
														UHU	ACINIO	VAIEH	DETAIL		
S	TALL	ATIC	N DE	TAIL	S				Date	Hole Depth	Casing Depth	Depth to Water	Com	ments					



## GEOTECHNICAL CORE LOG RECORD

REPORT NUMBER

22455

(25)		7															.240	
100	TR/	ACT	А	vid S	ite, Sand	dyford								LHOLE	NO	RC		
0	ORD	ANK	TES				-: 10.4		1				SHE				et 1 of	
RC	NIIC	DIF	VFI	(mOI	))				RIG TYPE		Geo4			COMP				
	ENT			arlet					FLUSH INCLINATI	ON (dea)	Air/Mi	st		LED BY		_	SL	
NG	INE	ER		ECO					CORE DIA				LOG	GED BY	,		.O'She	a
Down	Core Run Depth (m)	T.C.R.%	S.C.R.%	R.Q.D.%	Spa Lo (m	cture icing og im)	Non-intact Zone	Legend			Descript	ion			Depth (m)	Elevation	Standpipe Details	SPT (N Value)
2 3 4 5 5 7 7									SYMMETI as returns  SYMMETI as returns  SYMMETI as returns	RIX DRILL of grey br	ING: No recown black s	covery, obs andy grave covery, obs sandy GRA	erved by delly CLAY erved by delly CLAY	riller	0.90 2.20 3.20			
	10.5	<b>75</b>						0.000	SYMMETI as returns	RIX DRILL of grey bro	NG: No rec	overy, obs ilty sandy ç	erved by d ravelly CL	riller	9.40			
-	cas		.00-	11.30	m		***		ii <del>2 x sisi 24 -</del> i	Water	Casing	Sealed	Rise	Time	1	nmen		DETAILS
- 5										Strike	Depth	At	To	(min)				
															No	wate	r strike	record
											1				GRO	UND	VATER	DETAIL
	TALL	ATK	ON D	ETAII	LS					Date	Hole Depth	Casing Depth	Depth to Water	Com	ments			
IST									e		1 Debiii	Lenni	. FILLICI					



## GEOTECHNICAL CORE LOG RECORD

REPORT NUMBER

22455

co		ACT INA		viu S	ite, Sandyford			· · · · · · · · · · · · · · · · · · ·		vin	SHE	LHOLE	NO	RC She	04 et 2 of	2
				(mOI	))			RIG TYPE	Geo		100000	E COMP				
CLI	ENT		N	tarlet	A STATE OF THE STA	-		FLUSH INCLINATION (deg)	Air/N -90	list	DRIL	LED BY	,	IC	SSL	
	INE	ER	A	ECO	M		П	CORE DIAMETER (r	nm) 78		LOG	GED BY		D	.O'She	a
□ Downhole Depth (m)	Core Run Depth (m)	T.C.R.%	S.C.R.%	R.Q.D.%	Fracture Spacing Log (mm)	Non-intact Zone	Legend		Descrij	otion			Depth (m)	Elevation	Standpipe Details	SPT (N Value)
							K O     O	SYMMETRIX DRIL as returns of grey b	LING: No re rown sandy	covery, obs gravelly CL	erved by d AY	1	10.10			
2	-	The state of the s					1 + + + + + + + + + + + + + + + + + + +	SYMMETRIX DRIL as returns of probal	LING: No re	covery, obs ed ROCK	erved by d	riller	11.10			
1	2.60				_		+++	Probable Weathere	4 DOCK	accurated a	oond: av		12.60		H	
13							+++++++++++++++++++++++++++++++++++++++	cobbles of GRANIT	E - Non inta	ecovered as act	s sandy gra	avelly				
4		32	10	0	á		+++++++++++++++++++++++++++++++++++++++									
5	4.80						+	End of Boreho	le at 14.80	m	Walterman Salvanian distribution		14.80			
6																
7													0000			
8	-	umane.														
9																
EN	IARK	(S			11-11-11-11-11-11-11-11-11-11-11-11-11-					0 c			WAT	ED C	BIKE	DETAIL
			.00-1	1.30	m	-		Water Strike	Casing Depth	Sealed At	Rise To	Time (min)	1	nmen	************	
													No	o wate	er strike	record
			100,120-						Hole	Casing	Don't to	T	-		VATER	DETAI
market.	ALL	ATIC	ON D	ETAIL	S			Date	Depth	Judshig	Depth to Water	Com	ments			

### RC02 - Box 1 of 1 - 8.70-11.70m



### RC04 - Box 1 of 1 - 12.60-14.80m







### TRIAL PIT RECORD

REPORT NUMBER

22455

CON	TRACT	Avid Residential Development			blin			TRIAL PIT	NO.	Tp0	<b>1</b> t 1 of 1	
LOG	GED BY	S.Hannon	CO-ORDINA					DATE STA			3/2020 3/2020	
CLIE	NT NEER	Marlet Property Groupd Aecom	GROUND LE	VEL (m)				EXCAVA? METHOD		JCB		
								S	amples		a)	meter
		Geotechnical Descriptio	n	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Type	Depth	Vane Test (KPa)	Hand Penetrometer
0.0		GROUND - Tar GROUND - Dense sandy gravel.	Cravels are fine	<b>*****</b>	0.10							
	to coars	e and angular to sub rounded.		<b>*****</b>	0.30							
	content.	GROUND - Dense gravel with a high gravels are fine to coarse and g	nigh cobble gravels and		0.50			AA131830	В	0.50		
	Stiff gre	are angular to sub rounded. y light brown slightly silty very gra	avelly CLAY with						177	510.5		
	high cot	oble content and low boulder con oarse and gravels cobbles and b	tent. Gravels are oulders are	2				1				
1.0	angular	to sub rounded. Possible made of y light brown slightly silty very gra	ground.		1.10			AA131831	В	1.00		
	high cot	oble content and low boulder con oarse and gravels cobbles and b	tent. Gravels are	x								
	angular	to sub rounded.	ouiders are									
				夏								
				0								
2.0				×0				AA131832	В	2.00		
				×9								
	Stiff - ve	ry stiff dark grey slightly silty very	gravelly CLAY	80-	2.50							
	and gra	dium cobble content. Gravels are vels and cobbles are angular to s	tine to coarse sub rounded.	4 9								
3.0	End of T	rial Pit at 3.00m		* 4	3.00			AA131833	В	2.80		
4.0												
	ndwater ( age at 2 i	Conditions n.	e e e e e e e e e e e e e e e e e e e									
Stabi Stabi		Description and the second sec	TOTAL AND				<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>					
	ral Rema	rks location for services			, 4.m. to 2.4, to 1.0,			·				

REPORT NUMBER TRIAL PIT RECORD 22455 1531 TRIAL PIT NO. Tp02 CONTRACT Avid Residential Development - Avid Site , Sandyford , Dublin SHEET Sheet 1 of 1 CO-ORDINATES DATE STARTED 10/03/2020 LOGGED BY S.Hannon DATE COMPLETED 10/03/2020 GROUND LEVEL (m) **EXCAVATION** JCB CLIENT Marlet Property Groupd METHOD **ENGINEER** Aecom Hand Penetrometer (KPa) Samples Vane Test (KPa) Water Strike Geotechnical Description Elevation Depth (m) Depth Type MADE GROUND - very clayey gravel with occasional wood, plastic, concrete and metal pieces. Gravels are fine to coarse and angular to sub rounded. 0.40 Firm - stiff dark brown slightly silty gravelly CLAY. Gravels AA131834 B 0.50 are fine to coarse and angular to sub rounded. Possible made ground. 1.0 1.10 Stiff dark brown very gravelly CLAY with high cobble content and low boulder content. Gravels are fine to AA131835 B 1.10 coarse and gravels cobbles and boulders are angular to sub rounded. 2.0 AA131836 B 2.20 2.80 Stiff - very stiff dark grey gravelly CLAY with medium cobble content. Gravels are fine to coarse and gravels and cobbles are angular to sub rounded. 3.00 3.00 AA1318337 B End of Trial Pit at 3.00m **Groundwater Conditions** Dry 22455.GPJ IGSL\_GDT 23/3/20 Stability Stable General Remarks

CAT scanned location for services

IGSL TP LOG

15	ار دادة		TRIAL PIT	RECO	RD					REPORT N	umber 455	
CON	TRACT	Avid Residential Development	- Avid Site , Sand	yford , Du	blin			TRIAL PI	NO.	Tp0		
LOG	GED BY	S.Hannon	CO-ORDINA					DATE STA		10/0:	et 1 of 1 3/2020 3/2020	
CLIE	NT NEER	Marlet Property Groupd Aecom	GROUND LE	VEL (m)				EXCAVA* METHOD		JCB		
								S	Sample	es	)a)	meter
		Geotechnical Description	n	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Type	Depth	Vane Test (KPa)	Hand Penetrometer
0.0	plastic a medium	SROUND - Stiff brown very grave and metal pieces and high cobble boulder content. Gravels are fine cobbles and boulders are angula	content and to coarse and					AA131838	В	0.50		The state of the s
1.0	Stiff dark Gravels angular	k brown gravelly CLAY with low or are fine to coarse and gravels a to sub rounded.	obble content. nd cobbles are	010	0.90			AA131839	В	1.00		
2.0	content.	k brown very gravelly CLAY with Gravels are fine to coarse and g are angular to sub rounded.	medium cobble ravels and		1.40			AA131840	В	2.00		
3.0	End of T	rial Pit at 3.00m	and the state of t	ф IC	3.00			AA131841	В	3.00		
4.0												
<b>Grou</b> Dry	ndwater (	Conditions	on construction			100 E 100 E 100 E						Į.
Stabi Stabi			No. at A	u		-		U 100	<del>ernel</del> i		_+:	
	ral Rema	rks location for services						TO THE RESERVE TO THE PARTY OF				
J/11	-vailied !	Section for Jory1003										



### TRIAL PIT RECORD

REPORT NUMBER

22455

15	7.7.7.										
CON	TRACT Avid Residential Development - A	vid Site , Sandy	ford , Du	blin			TRIAL PI	T NO.	Tp0	4	
	OLE TO THE TENNES AND AND THE TENNES	Tanana					SHEET		Shee	t 1 of 1	
OG	GED BY S.Hannon	CO-ORDINAT	ES				DATE ST			3/2020	
		COOLINGIE					DATE CO	MPLET	ED 10/03	3/2020	
CLIE	NT Marlet Property Groupd	GROUND LE	VEL (M)				EXCAVA		JCB		
ENG	NEER Aecom						METHOD			Actoria	
											-
			1					Samples		ê	nete
						o o				Vane Test (KPa)	Hand Penetrometer (KPa)
	Geotechnical Description				E	Water Strike				est	ene
			end	5	Elevation	le le	age	Φ	ŧ	0	D &
			Legend	Depth (m)	E E	Wai	Sample Ref	Туре	Depth	Van	E A
0.0	MADE GROUND - very clayey gravel with o	ccasional	XXXXX				-				-
	wood, plastic, concrete and metal pieces. G	ravels are fine	<b>****</b>								
	to coarse and angular to sub rounded.		<b>****</b>								1
	Stiff dark brown you grountly CLAV with me	dium oobblo	<u> </u>	0.50			AA131842	В	0.50		
	Stiff dark brown very gravelly CLAY with me content. Gravels are fine to coarse and gra	vels and	0				AM 131044	В	0.50		
	cobbles are angular to sub rounded. Possib ground.	le made	2-0								
		northern the transfer and the	0_0	1.00							
1.0	Stiff dark brown very gravelly CLAY with me content and low boulder content. Gravels a	dium cobble	9	1.00			AA131843	В	1.00		
	coarse and gravels cobbles and boulders a	re angular to	9 0								
	sub rounded.		255								
			0-5								
			0								
			0								
2.0	Stiff - very stiff dark grey very gravelly CLAY	with medium	0	2.00			AA131844	В	2.00		
	cobble content and low boulder content. Gra	avels are fine	0								
	to coarse and gravels and cobbles are angurounded.	liar to sub	2								
6			~								
			0_0				AA131845	В	2.80		
	The second secon		0-	3.00			10104	ь	2.00		
3.0	End of Trial Pit at 3.00m										
4.0											
	ndwater Conditions		1			<u></u>	1 1				
Ory	idivater continuoris										
Stabi			**************	-			4 (1 94 10 4 100				
Stabl	e										

IGSL TP LOG 22455.GPJ IGSL.GDT 23/3/20

General Remarks
CAT scanned location for services

	الر <u>ائية</u> المائية	TRIAL PIT	RECO	RD	P				REPORT N	ивек 455	
CON	TRACT Avid Residential Development -	Avid Site , Sand	yford , Du	blin			TRIAL PIT	NO.		5 t 1 of 1	
LOG	GED BY S.Hannon	CO-ORDINA	TES				DATE ST		D 11/03	3/2020 3/2020	
CLIE	NT Marlet Property Groupd NEER Aecom	GROUND LE	VEL (m)				EXCAVAT METHOD		JCB		
							S	ample	es	<b>a</b>	meter
	Geotechnical Description		Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Туре	Depth	Vane Test (KPa)	Hand Penetrometer (KPa)
1.0	MADE GROUND very dense very gravelly occasional red brick metal plastic and con and high cobble content and medium boul	crete pieces					AA131846	В	0.50		
	Stiff dark brown slightly slity very gravelly (cobble content. Gravels are fine to coarse and cobbles are angular to sub rounded.	CLAY with high and gravels		1.20			AA131847	В	1.20		
2.0							AA131848	В	2.00		
	Stiff - very stiff dark grey gravelly CLAY wit content. Gravels are fine to coarse and gracobbles are angular to sub rounded.	th high cobble avels and	0 0	2.70							

4.0

Groundwater Conditions
Dry

Stability
Stable

General Rerr
CAT scanr General Remarks CAT scanned location for services



### TRIAL PIT RECORD

REPORT NUMBER

22455

LOG	GED BY S.Hannon  NT Marlet Property Groupd	CO-ORDINA GROUND LE					DATE ST. DATE CO	MPLET	11/03	8/2020 8/2020	
	NEER Aecom			T		1	METHOD				
							8	amples		Pa)	ometer
	Geotechnical Descripti	on	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Туре	Depth	Vane Test (KPa)	Hand Penetrometer (KPa)
0.0	MADE GROUND very gravelly sand wi content and medium boulder content. Of coarse and gravels cobbles and boulde sub rounded.	Fravels are fine to					AA131850	В	0.50		
1.0	Stiff slightly sandy very gravelly CLAY very content and low boulder content. Grave coarse and gravels cobbles and boulde sub rounded.	vith high cobble els are fine to ers are angular to	0.000.000	1.10			AA136803	В	1.10		
2.0				2.70			AA136804	В	2.00		
3.0	Stiff - very stiff dark grey very gravelly Cobble content. Gravels are fine to coal and cobbles are angular to sub rounder End of Trial Pit at 3.00m	se and gravels	φ <u>'</u> , φ'.	3.00		Schrift account has been strong and the strong and	AA136805	В	3.00		
4.0											A THE REAL PROPERTY AND A PROPERTY A
Dry	Indwater Conditions										
Stabi Stabi											
	eral Remarks scanned location for services	***************************************									

<u>ئ</u> اد	سرت ماقاد		TRIAL PIT	RECO	RD					REPORT N	имвек 455	
CON	TRACT	Avid Residential Development - A	Avid Site , Sandy	ford , Du	blin	***************************************		TRIAL PI	۲ NO.	Tp0		
LOG	GED BY	S.Hannon	CO-ORDINAT	ES		-6-		DATE ST		11/0	at 1 of 1 3/2020 3/2020	
CLIE	NT NEER	Marlet Property Groupd Aecom	GROUND LEY	VEL (m)				EXCAVAT METHOD		JCB		
								s	Sample	es	a)	neter
		Geotechnical Description		Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Туре	Depth	Vane Test (KPa)	Hand Penetrometer
0.0	MADE G	GROUND - Tar	Line	XXXX	0.10			1				
	content.	ROUND - very sandy gravel with h Gravels are fine to coarse and gra- are angular to sub rounded.	igh cobble vels and	<u> </u>	0.40							
	Stiff dark	c brown slightly silty very gravelly C cobble content. Gravels are fine to and cobbles are angular to sub rou	LAY with coarse and nded. Possible	0-0	0.60			AA136806	В	0.50		
1.0	Stiff dark	c brown very gravelly CLAY with me Gravels are fine to coarse and gra are angular to sub rounded.	edium cobble evels and	9/9/9				AA136807	В	1,00		
-				91919						-		
2.0				919 P				AA136808	В	2.00		
				19 PI 4 PI P				130000		2.00		
	Stiff - ve cobble c and cobl	ry stiff dark grey gravelly CLAY with ontent. Gravels are fine to coarse a bles are angular to sub rounded.	n medium and gravels	0 0	2.50							
3.0	End of T	rial Pit at 3.00m		-	3.00			AA136809	В	3.00		
4.0												
<b>Grou</b> Dry	ndwater 0	Conditions				at too						
O1,												
Stabi Stabi												
	ral Remai scanned l	rks ocation for services				- Control of the Cont					e Lord Table	

8	لىر		TRIAL PIT	RECO	RD					REPORT N	umber 455	
CON	TRACT	Avid Residential Development -	Avid Site , Sand	yford , Du	blin		***************************************	TRIAL PIT	NO.	Tp0		
LOG	GED BY	S.Hannon	CO-ORDINA					DATE STA		D 11/03	et 1 of 1 3/2020 3/2020	
CLIE	NT INEER	Marlet Property Groupd Aecom	GROUND LE	EVEL (m)				EXCAVAT METHOD	ION	JCB		
								S	ample	es	<sup>2</sup> a)	meter
		Geotechnical Description		Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Type	Depth	Vane Test (KPa)	Hand Penetrometer (KPa)
0.0	MADE of cobble of and cob Stiff light high col gravels	GROUND - Tar  GROUND - Dense very sandy graventent. Gravels are fine to coarse bles and are angular to sub round to brown slightly sandy very gravelled to content. Gravels are fine to coand cobbles are angular to sub ro	and gravels led. y CLAY with parse and unded.	0   0   0   0   0   0   0   0   0   0	0.10 0.30 0.70			AA136810	В	0.50		Action of the state of the stat
1.0	cobble	wn slightly sandy very gravelly cla content. Gravels are fine to coarse bles are angular to sub rounded.	y with high and gravels					AA136811	В	1.00		
2.0	cobble	ery stiff dark grey very gravelly CLA content. Gravels are fine to coarse bles are angular to sub rounded.	AY with high and gravels	0 0 0 0 0	2.00			AA136812	В	2.00		
3.0	End of	rial Pit at 3.00m		ф   c	3.00			AA136813	В	3.00		
4.0												
<b>Gro</b> u Dry	Indwater	Conditions	TATAMENTO CONTINUES POR ANCIONA									J.,
Stab Stab			serie di							al experience in the second deal even		
	eral Rema scanned	rks location for services		niima van		ntin petrinocus.		***************************************		147-41-0-77-0-0-0-47-47-1-2		

IGSL TP LOG 22455.GPJ IGSL,GDT 23/3/20

13	531	TRIAL PIT	RECO	RD					REPORT N	umber 455	
CON	ITRACT Avid Residential Development -	Avid Site , Sand	yford , Du	blin			TRIAL PI	ΓNO.	Tp0		
LOG	GED BY S.Hannon	CO-ORDINA					DATE ST		D 11/0:	at 1 of 1 3/2020 3/2020	
CLIE	NT Mariet Property Groupd INEER Aecom	GROUND LE	VEL (m)				EXCAVA METHOD		JCB		
								Sample	es	)a)	meter
	Geotechnical Description	è	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Туре	Depth	Vane Test (KPa)	Hand Penetrometer
0.0	MADE GROUND - Dense very sandy very with plastic concrete and metal pieces an content. Gravels are fine to coarse and gr cobbles and are angular to sub rounded.  Stiff light brown slightly silty very gravelly (cobble content. Gravels are fine to coarse	nd a high cobble ravels and	\$ 0 - 1	0.50			AA136814	В	0.50		
1.0	and cobbles are angular to sub rounded.						AA136815	В	1.00		
2.0	Stiff - very stiff dark grey very gravelly CLA cobble content and medium boulder conte fine to coarse and gravels cobbles and bo angular to sub rounded.	AY with medium ant. Gravels are sulders are		1.50			AA136816	В	2.00		THE STATE OF THE S
			9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3.00			AA136817	В	2.50		
4.0	End of Trial Pit at 3.00m										
Dry	andwater Conditions										
Stabi Stabi											
	eral Remarks scanned location for services			The second second				A service and			

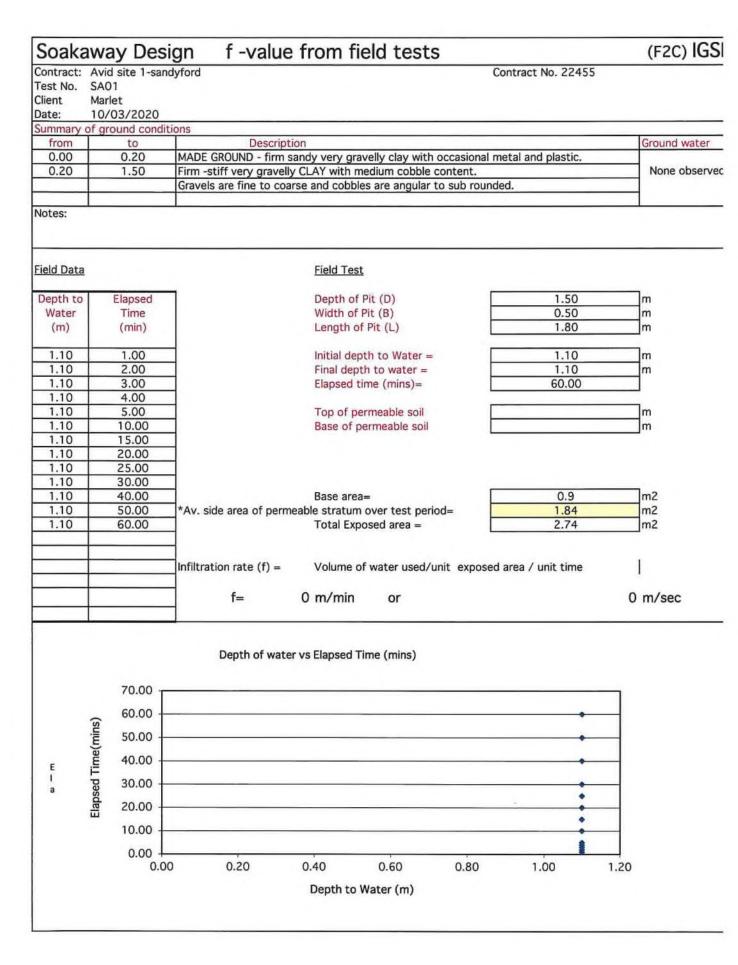
J s	سر 181		TRIAL PIT	RECO	RD					REPORT N	имвек 455	
CON	TRACT	Avid Residential Development	- Avid Site , Sand	yford , Du	blin			TRIAL PI	T NO.	Tp1		
LOG	GED BY	S.Hannon	CO-ORDINA				niesti, se e	DATE ST		11/0:	et 1 of 1 3/2020 3/2020	
CLIE	NT NEER	Marlet Property Groupd Aecom	GROUND LE	VEL (m)	(miles)			EXCAVA METHOD		JCB	***	
									Sample	s	oa)	meter
		Geotechnical Description	on	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Туре	Depth	Vane Test (KPa)	Hand Penetrometer
0.0	content. rounded Stiff brov Gravels	ROUND - very sandy gravel wit Gravels are fine to coarse and a wn very gravelly CLAY with high are fine to coarse and gravels a to sub rounded. Probable made	cobble content.	0,010,10   0,010,10	0.10			AA136818	В	0.50		
¯1.0	Gravels	wn very gravelly CLAY with high are fine to coarse and gravels a to sub rounded.	cobble content. nd cobbles are		0.70			AA136819	В	1.00		The same of the sa
20	Stiff - ver cobble c to coarse to sub ro	ry stiff dark grey very gravelly Cl ontent and low boulder content. e and gravels cobbles and bould bunded.	LAY with medium Gravels are fine ders are angular	00000000000000000000000000000000000000	1.80			AA136820	В	2.00		
					3.00			AA136821	В	2.50		
4.0	End of I	rial Pit at 3.00m										
Grou Dry Stabi		Conditions	3) H - A -						-			
Stabl												
	ral Remar scanned I	rks ocation for services				Tanadaria Herokania Araba	ng ngulaga sa manan	AND ANY OF THE PARTY OF THE PAR	in del ser dell'investion	a di periodica di serie di constituci	a and a by the street	

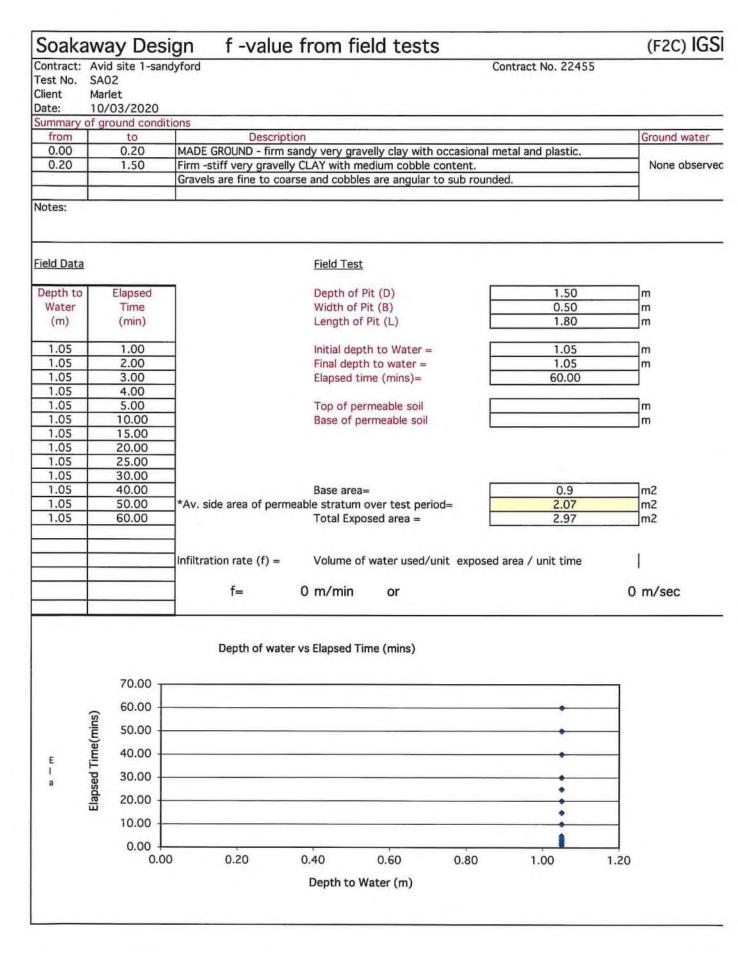
U S	ا برز		TRIAL PIT	RECO	RD					REPORT N	омвек 455	
CON	TRACT	Avid Residential Developmen	nt - Avid Site , Sand	yford , Du	blin		***************************************	TRIAL PI	T NO.	Tp1		
LOG	GED BY	S.Hannon	CO-ORDINA					DATE ST DATE CO		D 11/0:	et 1 of 1 3/2020 3/2020	
CLIE	NT NEER	Marlet Property Groupd Aecom	GROUND LE	VEL (m)				EXCAVA METHOD		JCB	- Marie Calif	
									Sample	es	)a)	meter
		Geotechnical Descript	ion	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Type	Depth	Vane Test (KPa)	Hand Penetrometer
0.0	medium gravels Stiff brow cobble of and cob- ground.		ne to coarse and o rounded. clay with high arse and gravels d. Probable made	φ. φ. φ.	0.10			AA136822	В	0.50		
1.0	content.	wn very gravelly CLAY with me Gravels are fine to coarse and are angular to sub rounded.	dium cobble gravels and	0 0 0 0 0 0				AA136823	В	1.00		
.0	cobble c	ery stiff dark grey very gravelly ( content and low boulder content e and gravels cobbles and bout bounded.	t. Gravels are fine		1.80			AA136824	В	2.00		
3.0	F-1-6				3.00			AA136825	В	2.50		
	Enu or i	rial Pit at 3.00m			And the latter of the latter o					terretina en estado e		
4.0										mention production and a service of the service of		
Grou	ndwater (	Conditions										
Stabi Stabi					erison Charles -	3 E mm						
	ral Remai scanned l	rks location for services		· · · · · · · · · · · · · · · · · · ·		STAN PORTONIAL	orion a real transaction	CALC 110 A 1.1				, <del>1</del>

		A STATE OF THE STA	TD141 D.		-				F	REPORT N	UMBER	
15	المرت		TRIAL PIT	RECO	RD					22	455	
CON	TRACT	Avid Residential Development	- Avid Site , Sand	yford , Du	blin			TRIAL PIT	NO.	Tp1		
OG	GED BY	S.Hannon	CO-ORDINA	TES	ng maning			DATE ST		11/03	t 1 of 1	
CLIE	NT	Marlet Property Groupd	GROUND LE	VEL (m)				DATE CO	TION	JCB	3/2020	
NGI	NEER	Aecom		T	T		T	METHOD	***********			
								S	amples	1	Pa)	ometer
		Geotechnical Description	1	Legend	Depth (m)	Elevation	Water Strike	Sample Ref	Type	Depth	Vane Test (KPa)	Hand Penetrometer
0.0	cobble (	GROUND dense very sandy grave content. Gravels are fine to coars	el with medium e and gravels	<b>****</b>	0.10							
	Stiff bro	obles are angular to sub rounded.  wn slightly sandy very gravelly cla  content. Gravels are fine to coars  obles are angular to sub rounded.	e and gravels	0_0	0.50			AA136826	В	0.50		
1.0	Stiff bro content cobbles	wn very gravelly CLAY with medion. Gravels are fine to coarse and goare angular to sub rounded.	ravels and	9 0 9	1.20			AA136827	В	1.00		
	to coars	ery stiff dark grey gravelly CLAY we content and high cobble content. see and gravels cobbles and bould conded.	Gravels are fine		1.20							
2.0	C114 1	ih. Olav			2.20			AA136828	В	2.00		
	cobble (	lowish orange silty gravelly CLAY content. Gravels are fine to coarsobles are angular to sub rounded.	e and gravels					AA136829	В	2.50		
3.0	End of	Trial Pit at 3.00m		×0 3	3.00			200				
40												
										3		
	ındwater	Conditions	Str. 18 - India 1	L			<u> </u>					
Dry												
Stabi Stabl												
2.12.50	Philippe Avenue											
	eral Rema scanned	irks location for services										









Appendix VI Laboratory Data

a. Geotechnical Soil and Rock

A CONTROL OF THE CONT	INAB	DIVILED IN SCORE SEG NO. 1720				Description	Brown sandy gravelly CLAY	Brown sandy gravelly CLAY	Brown sandy gravelly CLAY	Brown slightly sandy, slightly gravelly, CLAY	Brown sandy gravelly CLAY	Brown signity sandy, gravelty, CLAY	The state of the s			Programme enablinger in many enterpoints avoid y climate	¥	NOTE: *Clause 3.2 of BS1377 is a "withdrawn" standard due to publication of ISO17892-1:2014		혈	Date Page
			ndyford			Classification (BS5930)	CL			n TO	CL	CL						ard due to put	accreditation.	ining material	
	imits	4.4 & 5.3	opment Sa			Liquid Limit Clause	4.4	4.4	4.4	4.4	4.4	4.4						frawn" stands	the scope of	d. Any rema	ý
•	Determination of Moisture Content, Liquid & Plastic Limits	Tested in accordance with BS1377:Part 2:1990, clauses 3.2*, 4.3, 4.4 & 5.3	Avid Development Sandyford			Preparation	MS	MS	WS	WS	WS	SM					Hemarks: Results apply to the sample as received.	377 is a "witho	Opinions and interpretations are outside the scope of accreditation.	ecimens teste	Approved by
	Liquid &	i0, clauses				% <425µm	59	47	48	7.1	44	65					to the sampl	e 3.2 of BS1	interpretation	ate to the sp	
Test Report	Content,	:Part 2:199	Contract Name:			Plasticity	16	16	17	17	18	20					Hemarks: Results apply	NOTE: *Claus	Opinions and	The results re	
Tes	Moisture	th BS1377				Plastic Limit %	14	13	12	14	16	15									e reports
	nation of	ordance wi	22455		22/05/20	Liquid Limit %	30	59	29	31	34	35					B - Bulk Disturbed U - Undisturbed				zed to approv
	Determi	ested in acc			eq:	Moisture Content %	+	12	13	16	14	17					Sample Type:				Persons authorized to approve reports
		-	Contract No.		Date Tested:	Sample	-	8	В	В	В	8					 n		tive method	oint method	1.
				let	07/05/20	Lab. Ref	A20/1674	A20/1676	A20/1678	A20/1679	A20/1680	A20/1681					p p	Ö	4.3 Cone Penetrometer definitive method	4.4 Cone Penetrometer one point method	
			R111489	Aecom/Marlet		Depth (m)	3.0	3.0	3.0	8.0	3.0	0.9					 WS - Wet sieved AR - As received	NP - Non plastic	4.3 Cone Pene	4.4 Cone Pene	
oratory -	Unit J5, M7 Business Park Newhall, Naas	ı	Report No.	Customer	Samples Received:	Sample No. Depth (m)	135561	3	13553	13558	135083	130586					Preparation:		mit	Clause:	
IGSL Ltd Materials Laboratory	Unit J5, M7 Bu Newhall, Naas	Co. Kildare 045 846176				ВН/ТР	Bh01	Bh02	Bh03	Bh03	Bh04	Bh04					Notes:				0

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5 (note: Sedimentation stage not according)

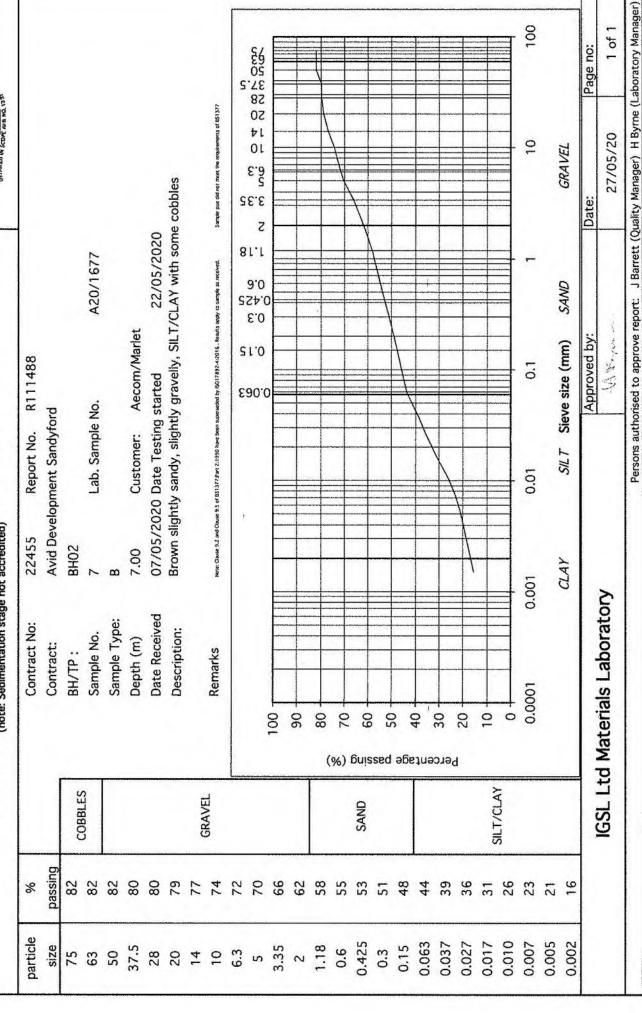


%		Contract No.	22455	Donort No	7971110			1
0	24	Contract No:	62455	Keport No.	K11148/			
passing		Contract:	Avid Develo	Avid Development Sandyford	D.			
001	COBBLES	BH/TP:	BH01					
3 5		Sample No.	135564	Lab. Sample No.	No.	A20/1675		
2 6	*******	sample Type:	20					
QQ.		Depth (m)	00.9	Customer:	Aecom/Marlet			
98		Date Received	07/05/202	07/05/2020 Date Testing started	started	22/05/2020		
80		Description:	Brown sligh	Brown slightly sandy, gravelly, SILT/CLAY	lly, SILT/CLAY			
92	CDAVE							
74	GRAVEL	Remarks	Note: Cruze 9.2 and Clause 9	.5 of 851.377.9srt 2:1990 have been as	haur Chure 9.2 and Chaue 9.5 of #51377 fint 2:1990 have been aupersories by \$017892-4:2016 . Realis 1999 is sample as received.	apply to sample as received.	Sample size did not need the requirements of 651377	
71			The state of the s		S	S		1 3
69					90.0	5.0 24.0 6.0	2.3.3.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.	20
29		100						
64		06						1
61		08					\ 	
58		202 (%)					1	
26	SAND	Co						
54	1				\ 	F		
50					7	•		
44				\ 				
39								1
36		20	1					
31	VA 12/ T 112	10						
56	SILI/CLAI	0						
23		0.0001	0.001	0.01	0.1	-	10	
21								
16		ř	CLAY	SILT Sie	Sieve size (mm)	SAND	GRAVEL	
	100				Approved by:		Date:	Page no:
	IGSL Ltd	IGSL Ltd Materials Laboratory	_		一个	I	27/05/20	

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5

(note: Sedimentation stage not accredited)





Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5 (note: Sedimentation stage not accredited)



particle size				- Contraction of the last of t	And the second s	The state of the s	Contraction of the last of the	The state of the s	The state of the s	-
	%		ප	Contract No:	22455	Report No.	R111486			
	passing		3	Contract:	Avid Devel	Avid Development Sandyford	- T-			
75	100	CORRIES	B	BH/TP:	BH03					
63	100		Sa	Sample No.	13558	Lab. Sample No.	No.	A20/1679		
20	100		Sa	Sample Type:	8		×			
37.5	100		De	Depth (m)	8.00	Customer:	Aecom/Marlet	a.r		
28	100		Da	Date Received	07/05/20	07/05/2020 Date Testing started	started	22/05/2020	0	
20	94		De	Description:	Brown sligi	Brown slightly sandy, slightly gravelly, CLAY	ly gravelly, CLA		d	
14	95	CDAVE								
10	91	GNAVEL	Re	Remarks	Note: Clara 9.2 and Claus	here: Chare 3.2 and Chaire 9.5 of 8513778412:1990 have been superhosed by ISO17892-43016 . Resalis Apply to sample as received.	persected by ISO17692-4:2016 . Resul	'us apply to sample as received.		
6.3	88			AND THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS	· ·	THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN THE PERSON NAMED		S		9
S	98						90.0	8.0 S4.0 8.0	2.3 5.6.3 10 10 14 20	20 28 37. 50 53
3.35	84		001					-		
2	78		- 06						1	
1.18	73		08							
9.0	29		- 02 (%)							
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0.3	63		sed				-			
0.15	09					_				
0.063	54									
0.038	47									
0.027	44		20 =							
0.017	39	VA 17/ T 112	10							
0.010	34	SELVCLAT	0							
0.007	31		0.0001		0.001	0.01	0.1	-	10	100
0.005	27									
0.002	19		14		CLAY	SILT Sie	Sieve size (mm)	SAND	GRAVEL	
		1 1001	111111111111				Approved by:		Date:	Page no:
		165L LT	IGSL LTD Materials Laboratory	Laborator	>		一个多字	9	27/05/20	1 of 1

Tested in accordance with: BS1377:Part2:1990, clause 9.2 & 9.5 (note: Sedimentation stage not accredited)



particle         %           size         passing           75         100           63         100           50         91           37.5         89           28         87           20         85           14         81           GRAVEL		Contract No:	22455	Report No.	R111490			
91 100 100 91 89 87 85 81								
100 100 91 89 87 85 85		Contract:	Avid Develo	Avid Development Sandyford	q			
100 91 89 87 85 85 79		BH/TP:	BH04					
91 88 87 85 81		Sample No.	130586	Lab. Sample No.	No.	A20/1681		
89 87 85 81 79		Sample Type:	В					
85 85 81 79		Depth (m)	6.00	Customer:	Aecom/Marlet			
85 81 79		Date Received	07/05/202	07/05/2020 Date Testing started	started	22/05/2020	0	
81 79		Description:	<b>Brown sligh</b>	Brown slightly sandy, gravelly, CLAY	lly, CLAY			
62								
		Remarks	Note: Clause 9.7 and Clause 5	Note: Claise 9.2 and Claise 8.5 of 651377 Fart 2:1990 have been supervised by 5017892.4:2016. Results spok to sample as received.	Perioded by 15017892-12016 - Resu	its apply to sample as received.	Surple and did not meet the requiements of 651377	2
		A SANDANGE AND SANDANG AND SAND	San			S		9
			1		90.0	8.0 S4.0 6.0	3.3 5.6 3.3 10 14 20	20 20 37. 50 50 50 50 50
		100				-		
19		06						1
18 58	(	80						
.6 55	(%)	70						
.25 54 SAND	6uis	09						
0.3 53	sed					+		
0.15 50	әбе	3			1			
0.063 46	tnə	04						
38 41	oerc	30						
0.027 38	1	20	1					
0.017 33 6.17.751		10						
28		0						
0.007 25		0.0001 0.	0.001	0.01	0.1	-	10	100
0.005 22	- 100 m							
0.002 15			CLAY	SILT Sie	Sieve size (mm)	SAND	GRAVEL	
- 1301					Approved by:		Date:	Page no:
IGSE I	to Mat	IGSL Ltd Materials Laboratory	>		一年を		28/05/20	1 of 1

		(Diametrial	) POINT LOAD ST	RENGTH	(Diametrial) POINT LOAD STRENGTH INDEX TEST DATA				(
Contract: Avid Site, Contract no. 22455 Date of test: 16/04	Contract: Avid Site, Sandyford Contract no. 22455 Date of test: 16/04/2020	lyford .0	Sample Type: Core	ore					
RC No.	Depth m	D (Diameter) mm	P (failure load)	ı.	ls (index strength) Mpa	Is(50) (index strength) Mpa	*UCS	Type	Orienation
RC02	8.8 10.9 12.8	87 78 78 78	8.0 10.0 4.0 1.0	1.222	1.31 0.66 0.16	1.61 2.01 0.20 0.20	32 4 4 4	סססס	***
Sta	Statistical Summary Data	nary Data	Is(50)	ncs*	*UCS Normal	*UCS Normal Distribution Curve	rve	Ab	Abbreviations
Number of San Minimum Average Maximum Standard Dev.	Number of Samples Tested Minimum Average Maximum Standard Dev.	p	4 0.20 1.15 2.01 0.81	4 4 40 40 16	0.12 0.08 0.06			- a D D	irregular axial block diametral
oper 95% C	Upper 95% Confidence Limit Lower 95% Confidence Limit	mit mit	2.74	54.82			TT	appro to weakr	approx. orientation to planes of weakness/bedding
Comments: *UCS taken a	Comments: *UCS taken as k x Point Load Is(50):	oad ls(50): k=		20	8-	0 200	300	⊃ a. 3	unknown perpendicular

Y

Appendix VI Laboratory Data

b. Chemical and Environmental





Chemtest Ltd.
Depot Road
Newmarket
CB8 0AL
Tel: 01638 606070

Email: info@chemtest.com

## **Final Report**

Report No.:

20-10240-1

Initial Date of Issue:

22-Apr-2020

Client

**IGSL** 

Client Address:

M7 Business Park

Naas

County Kildare

Ireland

Contact(s):

Darren Keogh

Project

22455 Avid Development Sandyford (

Aecom / Marlet )

Quotation No.:

Date Received:

08-Apr-2020

Order No.:

Date Instructed:

14-Apr-2020

No. of Samples:

21

Turnaround (Wkdays):

Results Due:

22-Apr-2020

Date Approved:

22-Apr-2020

Approved By:

Details:

Glynn Harvey, Technical Manager



Chemtest	The right chemistry to deliver results	Project: 22455 Avid Development Sandyford ( Aecom /

Marlet)																		
Client: IGSL	The state of the s	Towns !	Chen	ntest Jo.	5 No.: 2	Chemtest Job No.:   20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240
Quotation No.:		3	hemte	Chemtest Sample ID.:		996074	996075	920966	220966	820966	620966	080966	996081	996082	996083	996084	996085	996086
Order No.:			Clien	Client Sample Ref.:		131830	131831	131834	131838	131839	131842	131846	131847	131850	136807	136811	136814	136819
			Sa	Sample Location:	sation:	TP1	TP1	TP2	TP3	TP3	TP4	TP5	TP5	TP6	TP7	TP8	TP9	TP10
				Sample Type:	Type:	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL
			_	Top Depth (m):	:(ш) ц	0.50	1.00	0.50	0.50	1.00	0.50	0.50	1.20	0.50	1.00	1.00	0.50	1.00
			Bott	Bottom Depth (m):	h (m):	0.50	1.00	0.50	0.50	1.00	0.50	0.50	1.20	0.50	1.00	1.00	0.50	1.00
Determinand	Accred.	SOP	Type	Units	TOD												HE WAS TO SERVE	
Hd	n	1010	10:1		N/A	8.5	8.3	8.7	8.4	8.8	8.9	10.2	8.5	10.6	9.3	9.3	10.4	9.4
Ammonium	n	1220	10:1	I/gm	0.050	0.058	0.14	0.21	1.7	< 0.050	0.18	< 0.050	0.16	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
Ammonium	N	1220	10:1	mg/kg	0.10	69.0	1.6	2.7	19	0.48	2.5	0.64	1.9	0.63	0.85	0.30	0.52	0.25
Boron (Dissolved)	n	1450	10:1	l/gu	20	27	26	59	32	< 20	29	< 20	< 20	23	< 20	< 20	20	< 20
Boron (Dissolved)	n	1450	10:1	mg/kg	0.20	0.27	0.26	0.29	0.32	< 0.20	0.29	< 0.20	< 0.20	0.23	< 0.20	< 0.20	0.20	< 0.20



Client: IGSL			Cher	Chemtest Job No.:	b No.:	20-10240	20-10240	20-10240	
Quotation No.:		٠	Shemte	Chemtest Sample ID.:	ole ID.:	280966	880966	680966	
Order No.:			Clier	Client Sample Ref.:	le Ref.:	138822	136827	13559	
,			Sa	Sample Location:	cation:	TP11	TP12	BH1	
				Sample	Sample Type:	SOIL	SOIL	SOIL	
				Top Depth (m):	oth (m):	0.50	1.00	1.00	
			Bot	Bottom Depth (m):	th (m):	0.50	1.00	1.00	
Determinand	Accred.	SOP	Type	Units	LOD			STATE OF	
Hd	ח	1010	10:1		N/A	9.4	9.2	9.1	
Ammonium	ח	1220	10:1	l/gm	0.050	< 0.050	< 0.050	< 0.050	
Ammonium	z	1220	10:1	mg/kg	0.10	0.29	0.51	0.42	
Boron (Dissolved)	n	1450	10:1	l/gu	20	< 20	< 20	< 20	
Boron (Dissolved)	n	1450	10:1	mg/kg	0.20	< 0.20	< 0.20	< 0.20	



Quotation No.:         Chemte           Order No.:         Cilier           Order No.:         Cilier           Order No.:         Cilier           Determinand         Accred.         SOP           ACM Type         U         2192           AcM Detection Stage         U         2192           Moisture         U         2192           Moisture         N         2010           Boron (Hot Water Soluble)         N         2120           Sulphate (2:1 Water Soluble)         N         2120           Sulphur (Elemental)         M         2120           Chloride (Water Soluble)         M         2120           Nitrate (Water Soluble)         M         2120           Ocyanide (Total)         M         2220           Cyanide (Total)         M         2325           Ammonium (Water Soluble)         M         2430           Sulphate (Acid Soluble)         M         2430	Chemtest Sample ID.:		20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240
tification		nple ID.:	996074	996075	920966	220966	820966	996079	080966	996081	996082
and Accred. Soluble)  Ction Stage U 21  Ction Stage U 21  Ction Stage U 21  Ction Stage U 21  N 20  I Water Soluble) M 21  I Water Soluble) M 21  I Water Soluble) M 21  Mur Mater Soluble) M 21  Mur Mater Soluble) M 21  I Ction Stage U 22  I Water Soluble) M 21  I Ction Stage U 22  I Water Soluble) M 22  I Ction Stage U 22  I Water Soluble) M 22  I Ction Stage M 21  I Ction Stage U 22  I Ction Stage M 21	Client Sam	Client Sample Ref.:	131830	131831	131834	131838	131839	131842	131846	131847	131850
Accred. Sc U 21 U 21 U 21 U 21 N 20 Inble) M 21 Soluble) as SO4 M 21 (e) M 21 (h) M 22 (h) M 21 (h) M 21 (h) M 22 (h) M 21 (h) M 21 (h) M 21 (h) M 22 (h) M 21 (h) M 21 (h) M 22 (h) M 23 (h) M 23 (h) M 23 (h) M 23 (h) M 24 (h) M 25 (h) M 26 (h) M 27 (h) M 27	Sample Location:	ocation:	TP1	TP1	TP2	TP3	TP3	TP4	TP5	TP5	TP6
Accred. Sc U 21 U 21 U 21 U 21 N 20 Inble) M 21 Soluble) as SO4 M 21 (e) M 21 (h) M 22 (h) M 22 (h) M 21 (h) M 22 (h) M 21 (h) M 21 (h) M 21 (h) M 21 (h) M 21 (h) M 22 (h) M 22 (h) M 23 (h) M 23 (h) M 24 (h) M 25 (h) M 26 (h) M 27 (h) M 27	Sami	Sample Type:	SOIL								
Accred. Sc U 21 U 21 U 21 U 21 N 20 Iuble) M 21 Iuble) M 22 Iuble) M 22 Iuble) M 22 Iuble) M 22 Iuble) M 22 Iuble) M 23 Iuble) M 24 Iuble) M 25 Iuble) M 26 Iuble) M 27 Iuble) M 27 Iu	Top D	Top Depth (m):	0.50	1.00	0.50	0.50	1.00	0.50	0.50	1.20	0.50
Accred. Sc U 21 U 21 U 21 U 21 U 21 N 20 Iuble) M 21 ioluble) as SO4 M 21 M 21 ioluble) as SO4 M 21 M 21 ioluble) M 22 ioluble) M 21 ioluble) M 21 ioluble) M 22 ioluble) M 22 ioluble) M 22 ioluble) M 22 ioluble) M 22 ioluble) M 22 ioluble) M 23 ioluble) M 24 ioluble) M 25 ioluble) M 26 ioluble) M 27 ioluble)	Bottom Depth (m):	epth (m):	0.50	1.00	0.50	0.50	1.00	0.50	0.50	1.20	0.50
Accred.  U U U U U N Intele) M Intele) M Intele) M M Intele) M M Intele) M M M M M Intele) M M M M Intele) M M M M M Intele) M M M M M Intele) M M M M M M M M M M M M M M M M M M M	Asbe	Asbestos Lab:	COVENTRY								
U U U U U U U U U U U U U U U U U U U	OP Units	COD			STREET STREET					THE REAL PROPERTY.	The state of the
oluble) as SO4 M (elb)		N/A		t							-
ouble)	92 %	0.001	No Asbestos Detected								
oluble) M M M M M M M M M M M M M M M M M M M	92	N/A			,						
z	30 %	0.020	15	16	12	13	8.6	8.2	5.9	17	7.3
S Z S S S S Z S Z S S	10	4.0									
z	20 mg/kg	3 0.40	0.68	0.49	< 0.40	0.48	< 0.40	< 0.40	< 0.40	0.42	0.53
S S S S Z S Z S S	20 g/l	0.010									
S S S Z S Z S S	20 g/l	0.010									
S S Z S Z S S		0.010									
S Z S Z S S	80 mg/kg	1.0	[A] 3.7	[A] < 1.0							
ZZZZZ	20 g/l	0.010									
∑ Z ∑ ∑	20 g/l	0.010									
zΣΣ	100 mg/kg		[A] < 0.50								
M (aldı	125 mg/kg	3 0.50	[A] 3.2	[A] 2.2	[A] 8.1	[A] 9.2	[A] 5.2	[A] 6.5	[A] 7.1	[A] 2.1	[A] 7.2
M	20 g/l	0.01									
	30 %	0.010	[A] 0.074	[A] 0.015	[A] 0.029	[A] 0.054	[A] 0.031	[A] 0.038	[A] 0.45	[A] 0.045	[A] 0.11
	50 mg/kg	1.0	18	14	21	20	24	22	18	14	20
	50 mg/kg	9 10	120	86	71	91	46	47	49	89	61
	2450 mg/kg	g 0.10	2.1	1.1	2.4	2.9	1.6	2.1	0.67	2.6	1.2
Chromium M 2450	50 mg/kg	1.0	21	26	16	18	13	12	15	20	20
	50 mg/kg	3 2.0	2.8	2.8	3.5	3.4	2.9	3.7	< 2.0	3.9	< 2.0
П	50 mg/kg	3 2.0	< 2.0	< 2.0	2.0	2.1	< 2.0	< 2.0	< 2.0	2.2	< 2.0
Copper M 2450	50 mg/kg	3 0.50	27	21	26	32	20	22	15	29	19
	2450 mg/kg	_	0.17	0.15	< 0.10	0.16	< 0.10	< 0.10	< 0.10	0.11	< 0.10
	2450 mg/kg	_	41	39	48	53	37	41	22	56	32
	2450 mg/kg	_	59	34	31	84	19	21	12	28	17
	2450 mg/kg	-	0.83	0.50	0.35	0.54	< 0.20	0.29	< 0.20	0.63	< 0.20
W	2450 mg/kg	9 0.50	63	140	98	66	69	29	52	110	89
Chromium (Trivalent) N 249	2490 mg/kg	$\overline{}$	21	26	16	18	13	12	15	20	20
Chromium (Hexavalent) N 2490		g 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
Total Organic Carbon M 2625	325 %	0.20	[A] 1.6	-[A] 0.50	[A] 0.52	[A] 0.98	[A] 0.35	[A] 0.35	[A] 0.31	[A] 0.61	[A] < 0.20
Mineral Oil N 2670	370 mg/kg	g 10	< 10	< 10	< 10	< 10	< 10	< 10	150	< 10	< 10
z	2680 mg/kg	9 1.0	[A] < 1.0								
z	2680 mg/kg	_	[A] < 1.0								
M	2680 mg/kg	_	[A] < 1.0								
-	2680 mg/kg	g 1.0	[A] < 1.0								



Client: IGSL Chemtest		Chei	Chemtest Job No.:	No.:	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240
Quotation No.:		Chemte	Chemtest Sample ID.:	e ID.:	996074	996075	986076	220966	820966	996079	080966	996081	996082
Order No.:		Clie	Client Sample Ref.:	Ref.:	131830	131831	131834	131838	131839	131842	131846	131847	131850
		SS	Sample Location:	ation:	TP1	TP1	TP2	TP3	TP3	TP4	TP5	TP5	TP6
			Sample Type:	Type:	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL
			Top Depth (m):	.(m)	0.50	1.00	0.50	0.50	1.00	0.50	0.50	1.20	0.50
		Bot	Bottom Depth (m):	n (m):	0.50	1.00	0.50	0.50	1.00	0.50	0.50	1.20	0.50
			Asbestos Lab:		COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY
Determinand	Accred.	SOP	Units	COD					100	COATE LESS			ALC: NO SE
Aliphatic TPH >C12-C16	Σ	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aliphatic TPH >C16-C21	M	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aliphatic TPH >C21-C35	M	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aliphatic TPH >C35-C44	z	2680		1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Total Aliphatic Hydrocarbons	z	2680	mg/kg	5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0
Aromatic TPH > C5-C7	z	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH >C7-C8	z	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH >C8-C10	W	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH >C10-C12	Σ	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH >C12-C16	Σ	2680		1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH >C16-C21	כ	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH >C21-C35	Σ	2680	ma/ka	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Aromatic TPH > C35-C44	z	2680	ma/ka	10	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0					
Total Aromatic Hydrocarbons	z	2880	mo/kg	202	[4] < 5.0	[4] < 5.0	[4] < 5.0	[4] < 5.0	[A] < 5.0	[4] < 5.0	[4] < 5.0	[4] < 5.0	[4] < 5.0
Total Detroloum Lydrocarbons	2	2880	Bullen Bullen	100	100 40	[A] < 40	[A] 40	TA1 410	101710	101740	101740	200 (4)	101 - 40
Total Petroleum Hydrocalbons	2 2	2260	By/Bill	2.0	201710	01 / [2]	2017 101	01 / [0]	01 / [4]	27.10	(A) 10	[A] × 10	[A] > [O]
Benzene	Σ	2/00		2 .	(A) < 1.0	(A) < 1.0	0.1 × (A)	0.1 > [A]	(A) < 1.0	(A) < 1.0	(A) < 1.0	0.1 × [A]	0.1 > (A)
Toluene	Σ	2760		1.0	A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	(A) < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Ethylbenzene	Σ	2760		1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
m & p-Xylene	Σ	2760	µg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
o-Xylene	M	2760		1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Methyl Tert-Butyl Ether	W	2760		1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0
Naphthalene	W	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Acenaphthylene	z	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Acenaphthene	W	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Fluorene	M	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Phenanthrene	M	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Benzo[j]fluoranthene	z	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Anthracene	M	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Fluoranthene	M	2800	mg/kg	0.10	0.19	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Pyrene	Σ	2800	mg/kg	0.10	0.17	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Benzo[a]anthracene	Σ	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Chrysene	Σ	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Benzo[b]fluoranthene	Σ	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Benzo[k]fluoranthene	Σ	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Benzo[a]pyrene	Σ	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Indeno(1,2,3-c,d)Pyrene	Σ	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10
Dibenz(a,h)Anthracene	z	2800	mg/kg	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10

1



[A] < 0.010 [A] < 0.010[A] < 0.010 [A] < 0.010[A] < 0.010 [A] < 0.010[A] < 0.10COVENTRY [A] < 0.010131850 996082 < 0.10 < 0.10 < 0.30 SOIL 0.50 TP6 COVENTRY [A] < 0.010[A] < 0.010[A] < 0.010[A] < 0.010 [A] < 0.010 [A] < 0.010 [A] < 0.010[A] < 0.1020-10240 < 0.10 131847 < 0.30 < 0.10 996081 < 2.0 TP5 SOIL 1.20 COVENTRY [A] < 0.010[A] < 0.010[A] < 0.010 [A] < 0.010[A] < 0.010 [A] < 0.010 [A] < 0.010 [A] < 0.1020-10240 131846 < 0.10 996080 < 0.10 < 2.0 < 0.30 TP5 SOIL 0.50 0.50 [A] < 0.010 [A] < 0.010 [A] < 0.010 [A] < 0.010 [A] < 0.010[A] < 0.010 COVENTRY [A] < 0.010[A] < 0.10 20-10240 131842 < 0.30 996079 < 0.10 < 0.10 SOIL 0.50 < 2.0 TP4 0.50 [A] < 0.010 [A] < 0.010COVENTRY [A] < 0.010 [A] < 0.010[A] < 0.010 [A] < 0.010[A] < 0.010 [A] < 0.1020-10240 131839 < 0.10 996078 < 0.10 < 0.30 < 2.0 1.00 TP3 SOIL 1.00 [A] < 0.010 [A] < 0.010[A] < 0.010 [A] < 0.010COVENTRY [A] < 0.010[A] < 0.10 [A] < 0.010[A] < 0.010 20-10240 131838 < 0.10 < 0.30 < 0.10 996077 SOIL 0.50 < 2.0 0.50 COVENTRY [A] < 0.010 [A] < 0.010[A] < 0.010[A] < 0.10 20-10240 131834 < 0.10 920966 < 0.10 < 0.30 < 2.0 SOIL 0.50 0.50 COVENTRY [A] < 0.010 [A] < 0.10 20-10240 < 0.10 131831 996075 < 0.10 < 2.0 < 0.30 SOIL 1.0 TP1 1.00 COVENTRY [A] < 0.010 [A] < 0.1020-10240 < 0.10 131830 996074 < 0.10 < 2.0 < 0.30 SOIL 0.50 0.50 Chemtest Job No.: Asbestos Lab: 2815 mg/kg 0.010 2815 mg/kg 0.010 2815 mg/kg | 0.010 2815 mg/kg 0.010 Chemtest Sample ID.: Sample Location: Sample Type: 2815 mg/kg 0.010 2815 mg/kg 0.010 2815 mg/kg 0.010 Client Sample Ref .: Top Depth (m): Bottom Depth (m): 2800 mg/kg 0.10 2800 mg/kg 0.10 0.10 2920 mg/kg 0.30 SOP Units LOD 2.0 2800 mg/kg 2815 mg/kg Project: 22455 Avid Development Sandyford ( Aecom / Marlet ) Accred. Σ z Total PCBs (7 Congeners) Benzo[g,h,i]perylene Total Of 17 PAH's Quotation No.: Total Phenols Determinand PCB 90+101 Client: IGSI Order No.: Coronene PCB 118 PCB 138 PCB 153 PCB 180 PCB 28 PCB 52



Client: IGSL	Client: IGSL Chemtest.	Cher	Chemtest Job No.:	b No.:	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240
Quotation No.:	Ö	hemtes	Chemtest Sample ID.:	le ID.:	996083	996084	996085	980966	280966	880966	680966	060966	996091
Order No.:		Clien	Client Sample Ref .:	e Ref.:	136807	136811	136814	136819	138822	136827	13559	135560	-
		Sal	Sample Location:	cation:	TP7	TP8	TP9	TP10	TP11	TP12	BH1	BH1	BH2
			Sample Type:	: Type:	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL
			Top Depth (m)	th (m):	1.00	1.00	0.50	1.00	0.50	1.00	1.00	2.00	1.00
		Bott	Bottom Depth (m):	th (m):	1.00	1.00	0.50	1.00	0.50	1.00	1.00	2.00	1.00
			Asbestos Lab:	s Lab:	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY		
Determinand	Accred.		Units	LOD	A CONTRACTOR OF THE PARTY OF TH						AND REAL PROPERTY.		100
ACM Type	n	2192		N/A				· ·					
Asbestos Identification	ם	2192	%	0.001	No Asbestos Detected	No Asbestos Detected	No Asbestos Detected	No Asbestos Detected	No Asbestos Detected	No Asbestos Detected	No Asbestos Detected		
ACM Detection Stage	n	2192		N/A		,		ï	ï				
Moisture	z	2030	%	0.020	11	9.1	8.5	10	9.1	10	10	12	12
pH (2.5:1)	П		_	4.0								[A] 8.6	[A] 8.7
Boron (Hot Water Soluble)		$\overline{}$	6	0.40	< 0.40	< 0.40	< 0.40	< 0.40	< 0.40	< 0.40	< 0.40		
Magnesium (Water Soluble)	z	2120	T	0.010								< 0.010	< 0.010
Sulphate (2:1 Water Soluble) as SO4	7	2120	T	0.010								< 0.010	< 0.010
Total Sulphur				0.010	- 1							[A] 0.033	[A] 0.036
Sulphur (Elemental)	1		mg/kg	0.1	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Chloride (Water Soluble)		2220	$\neg$	0.010								[A] < 0.010	[A] < 0.010
Nitrate (Water Soluble)		2220	l/g	0.010								< 0.010	< 0.010
Cyanide (Total)			mg/kg	0.50	[A] < 0.50	[A] < 0.50	[A] < 0.50	[A] < 0.50	[A] < 0.50	[A] < 0.50	[A] < 0.50		
Sulphide (Easily Liberatable)			mg/kg	0.50	(A) 6.6	[A] 7.8	[A] 9.3	[A] 8.3	[A] 8.3	[A] 7.6	[A] 6.6		
Ammonium (Water Soluble)		2120	7	0.01								0.02	0.04
Sulphate (Acid Soluble)			_	0.010	[A] 0.011	[A] 0.013	[A] 0.083	[A] 0.012	[A] 0.033	[A] 0.010	[A] 0.017	[A] 0.018	[A] < 0.010
Arsenic			mg/kg	1.0	23	22	23	23	24	21	23		
Barium			mg/kg	10	71	63	65	100	20	62	71		
Cadmium			mg/kg	0.10	2.3	1.9	1.2	2.0	1.8	2.0	2.0		
Chromium		2450	mg/kg	1.0	15	13	15	15	14	14	14		
Molybdenum		2450	mg/kg	2.0	3.4	3.4	2.5	3.7	3.4	3.6	3.5		
Antimony	z	2450	mg/kg	2.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0		
Copper			mg/kg	0.50	56	22	19	26	23	56	26		
Mercury			mg/kg	0.10	< 0.10	< 0.10	0.11	< 0.10	< 0.10	< 0.10	< 0.10		
Nickel		2450	mg/kg	0.50	51	41	32	47	42	46	46		
Lead			mg/kg	0.50	21	18	20	19	23	18	19		
Selenium	M		mg/kg	0.20	< 0.20	0.41	0.30	1.4	0.24	1.6	0.37		
Zinc	M		mg/kg	0.50	79	76	64	76	29	75	74		
Chromium (Trivalent)	z	2490	mg/kg	1.0	15	13	15	15	14	14	14		
Chromium (Hexavalent)	Z		mg/kg	0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50		
Total Organic Carbon	M	2625	%	0.20	[A] 0.28	[A] 0.35	[A] 0.56	[A] 0.38	[A] 0.31	[A] 0.34	[A] 0.34		
Mineral Oil	z	2670	mg/kg	10	< 10	< 10	< 10	< 10	< 10	< 10	< 10		
Aliphatic TPH >C5-C6	z	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aliphatic TPH >C6-C8	z	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aliphatic TPH >C8-C10	M	2680	mg/kg	1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		



Client: IGSL	STATE OF THE PERSON NAMED IN	Chei	Chemtest Job No .:	0.: 20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240
Quotation No.:		hemte	Chemtest Sample ID.:	D.: 996083	996084	996085	980966	996087	880966	680966	060966	996091
Order No.:		Clie	Client Sample Ref .:		136811	136814	136819	138822	136827	13559	135560	-
		Ss	Sample Location:	on: TP7	TP8	TP9	TP10	TP11	TP12	BH1	BH1	BH2
			Sample Type:	L	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL	SOIL
			Top Depth (m):	n): 1.00	1.00	0.50	1.00	0.50	1.00	1.00	2.00	1.00
		Bot	Bottom Depth (m):	1.00	Н	0.50	1.00	0.50	1.00	1.00	2.00	1.00
				ab: COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY	COVENTRY		
Determinand	Accred.	SOP	Units LOD			Bush of the land				The state of the s	State of the State	
Aliphatic TPH >C12-C16	M	2680	mg/kg 1.0	0 [A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aliphatic TPH >C16-C21	W	2680	mg/kg 1.0	L	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aliphatic TPH >C21-C35	W	2680	mg/kg 1.0	L	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aliphatic TPH >C35-C44	z	2680	mg/kg 1.0	H	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Total Aliphatic Hydrocarbons	z	2680	mg/kg 5.0	) [A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0		
Aromatic TPH >C5-C7	z	2680	mg/kg 1.0	L	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aromatic TPH >C7-C8	z	2680	mg/kg 1.0	Н	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aromatic TPH >C8-C10	M	2680	mg/kg 1.0	_	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aromatic TPH >C10-C12	M	2680	mg/kg 1.0	Н	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aromatic TPH >C12-C16	M	2680	mg/kg 1.0	_	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
romatic TPH >C16-C21	n	2680	mg/kg 1.0	Н	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aromatic TPH >C21-C35	M	2680	mg/kg 1.0	_	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Aromatic TPH >C35-C44	z	2680	mg/kg 1.0	Н	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Total Aromatic Hydrocarbons	Z	2680	mg/kg 5.0	4	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0	[A] < 5.0		
Total Petroleum Hydrocarbons	z	2680	mg/kg 10.0	_	[A] < 10	[A] < 10	[A] < 10	[A] < 10	[A] < 10	[A] < 10		
Benzene	M	2760	µg/kg 1.0	[A] < 1	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Toluene	M	2760	1.0 Jg/kg	[A] < 1	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Ethylbenzene	M	2760	µg/kg 1.0	[A] < 1	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
m & p-Xylene	Σ	2760	µg/kg	[A] < 1	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
o-Xylene	Σ	2760		0 [A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Methyl Tert-Butyl Ether	Σ	2760	µg/kg	[A] < 1	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0	[A] < 1.0		
Naphthalene	Σ	2800	mg/kg	4	< 0.10	0.14	< 0.10	< 0.10	< 0.10	< 0.10		
Acenaphthylene	z	2800	mg/kg	4	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10		
Acenaphthene	Σ	2800	mg/kg		< 0.10	0.31	< 0.10	< 0.10	< 0.10	< 0.10		
Fluorene	Σ	2800	mg/kg	Ц	< 0.10	0.19	< 0.10	< 0.10	< 0.10	< 0.10		
Phenanthrene	Σ	2800	mg/kg		< 0.10	1.7	< 0.10	< 0.10	< 0.10	< 0.10		
Benzo[j]fluoranthene	z	2800	mg/kg	0 < 0.10	< 0.10	0.27	< 0.10	< 0.10	< 0.10	< 0.10		
Anthracene	M	2800	mg/kg		< 0.10	0.25	< 0.10	< 0.10	< 0.10	< 0.10		
Fluoranthene	Σ	2800	mg/kg 0.10	0 < 0.10	< 0.10	1.5	< 0.10	< 0.10	< 0.10	< 0.10		
Pyrene	M	2800	mg/kg 0.10	0 < 0.10	< 0.10	1.5	< 0.10	< 0.10	< 0.10	< 0.10		
Benzo[a]anthracene	M	2800	mg/kg 0.10	0 < 0.10	< 0.10	0.51	< 0.10	< 0.10	< 0.10	< 0.10		
Chrysene	Σ	2800	mg/kg 0.10	0 < 0.10	< 0.10	0.53	< 0.10	< 0.10	< 0.10	< 0.10		
Benzo[b]fluoranthene	M	2800	mg/kg		< 0.10	0.56	< 0.10	< 0.10	< 0.10	< 0.10		
Benzo[k]fluoranthene	M	2800	mg/kg		< 0.10	0.25	< 0.10	< 0.10	< 0.10	< 0.10		
Benzo[a]pyrene	M	2800	mg/kg		< 0.10	0.54	< 0.10	< 0.10	< 0.10	< 0.10		
Indeno(1,2,3-c,d)Pyrene	Σ	2800	2800 mg/kg 0.10	0 < 0.10	< 0.10	0.27	< 0.10	< 0.10	< 0.10	< 0.10		
		-							1			



Client: IGSL		Chem	Chemtest Job No.:		20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240	20-10240
Quotation No.:		Chemtes	Chemtest Sample ID.:		996083	996084	996085	980966	780966	880966	680966	060966	996091
Order No.:		Clien	Client Sample Ref .:		136807	136811	136814	136819	138822	136827	13559	135560	+
		Sar	Sample Location:	L	TP7	TP8	TP9	TP10	TP11	TP12	BH1	BH1	BH2
			Sample Type:	Type:	SOIL	SOIL							
			Top Depth (m):	:(m) t	1.00	1.00	0.50	1.00	0.50	1.00	1.00	2.00	1.00
		Botte	Bottom Depth (m):	:(m) t	1.00	1.00	0:20	1.00	0.50	1.00	1.00	2.00	1.00
			Asbestos Lab:		COVENTRY								
Determinand	Accred.	SOP	Accred.   SOP   Units   LOD	TOD								STEEL STEEL STEEL	
Benzo[g,h,i]perylene	M	2800	2800 mg/kg 0	0.10	< 0.10	< 0.10	0.37	< 0.10	< 0.10	< 0.10	< 0.10		
Coronene	z	2800	2800 mg/kg 0	0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10		
Total Of 17 PAH's	z	2800	2800 mg/kg	2.0	< 2.0	< 2.0	8.7	< 2.0	< 2.0	< 2.0	< 2.0		
PCB 28	n	2815	2815 mg/kg 0.010		[A] < 0.010								
PCB 52	n	2815	2815 mg/kg 0.010		[A] < 0.010								
PCB 90+101	ס	2815	2815 mg/kg 0.010		[A] < 0.010								
PCB 118	ח	2815	2815 mg/kg 0.010		[A] < 0.010								
PCB 153	ח	2815	2815 mg/kg 0.010		[A] < 0.010								
PCB 138	n	2815	2815 mg/kg 0.010		[A] < 0.010								
PCB 180	n	2815	2815 mg/kg 0.010		[A] < 0.010								
Total PCBs (7 Congeners)	n	2815	2815 mg/kg 0.10		[A] < 0.10								
Total Phenols	M	2920	2920 mg/kg 0.30	0.30	< 0.30	< 0.30	< 0.30	< 0.30	< 0.30	< 0.30	< 0.30		



Client: IGSL		Chei	ntest J	Chemtest Job No.:	20-10240	20-10240	20-10240
Quotation No.:		Shemte	Chemtest Sample ID.:	ple ID.:		860966	996094
Order No.:		Clier	Client Sample Ref .:	le Ref .:	13551	13553	130581
		Se	imple Lo	Sample Location:	BH3	BH3	BH4
			Sampl	Sample Type:	SOIL	SOIL	SOIL
			Top De	Top Depth (m):	1.00	3.00	1.00
		Bot	tom Deg	Bottom Depth (m):	1.00	3.00	1.00
			Asbest	Asbestos Lab:			
Determinand	Accred.	SOP	Units	LOD	The second second		
ACM Type	Э	2192		N/A			
Asbestos Identification	ס	2192	%	0.001			
ACM Detection Stage	>	2192		N/A			
Moisture	z	2030	%	0.020	18	12	10
pH (2.5:1)	z	2010		4.0	[A] 8.4	[A] 8.5	[A] 8.5
Boron (Hot Water Soluble)	M	2120	mg/kg	0.40			
Magnesium (Water Soluble)	z	2120	l/6	0.010	< 0.010	< 0.010	< 0.010
Sulphate (2:1 Water Soluble) as SO4	M	2120	l/b	0.010	< 0.010	< 0.010	< 0.010
Total Sulphur	Σ	2175	%	0.010	[A] 0.055	[A] 0.11	[A] 0.044
Sulphur (Elemental)	M	2180	mg/kg	1.0			
Chloride (Water Soluble)	M	2220	l/6	0.010	[A] < 0.010	[A] < 0.010	[A] < 0.010
Nifrate (Water Soluble)	z	2220	l/6	0.010	< 0.010	< 0.010	< 0.010
Cyanide (Total)	M	2300	mg/kg	_			
Sulphide (Easily Liberatable)	z	2325	mg/kg				
Ammonium (Water Soluble)	Σ	2120	l/g	0.01	2.8	0.07	0.03
Sulphate (Acid Soluble)	Σ	2430	%	0.010	[A] 0.027	[A] < 0.010	[A] 0.022
Arsenic	Σ	2450	mg/kg	1.0			
Barium	M	2450	mg/kg				
Cadmium	Σ	2450	mg/kg	0.10			
Chromium	M	2450	mg/kg				
Molybdenum	Σ	2450	mg/kg				
Antimony	Z	2450	mg/kg	2.0			
Copper	M	2450	mg/kg	0.50			-
Mercury	M	2450	mg/kg				
Nickel	M	2450	mg/kg	0.50	1		
Lead	M	2450	mg/kg	0.50			
Selenium	M	2450	mg/kg	0.20			
Zinc	M	2450	mg/kg	0.50			
Chromium (Trivalent)	z	2490	mg/kg				
Chromium (Hexavalent)	z	2490	mg/kg	0.50			
Total Organic Carbon	M	2625	%	0.20			
Mineral Oil	z	2670	mg/kg	10			
Aliphatic TPH >C5-C6	z	2680	mg/kg	1.0			
Aliphatic TPH >C6-C8	z	2680	mg/kg	1.0			
Aliphatic TPH >C8-C10	M	2680	mg/kg	1.0			
Alinhatic TPH >C10,C12	N	2680	mg/kg	1.0			



Client: IGSL	THE SECOND	Cher	Chemtest Job No.:	: oN do	20-10240	20-10240	20-10240
Quotation No.:		Shemte	Chemtest Sample ID.:	ple ID.:	996092	996093	996094
Order No.:		Clier	Client Sample Ref.:	le Ref.:	13551	13553	130581
		Ss	Sample Location:	cation:	BH3	BH3	BH4
			Sampl	Sample Type:	SOIL	SOIL	SOIL
			Top Depth (m):	oth (m):	1.00	3.00	1.00
		Bot	Bottom Depth (m):	oth (m):	1.00	3.00	1.00
			Asbest	Asbestos Lab:			
Determinand	Accred.	SOP	Units	TOD			
Aliphatic TPH >C12-C16	W	2680	mg/kg	1.0			
Aliphatic TPH >C16-C21	W	2680	mg/kg	1.0			
Aliphatic TPH >C21-C35	M	2680	mg/kg	1.0			
Aliphatic TPH >C35-C44	z	2680	mg/kg	1.0			
Total Aliphatic Hydrocarbons	z	2680	mg/kg	5.0			
Aromatic TPH >C5-C7	z	2680	mg/kg	1.0			
Aromatic TPH >C7-C8	z	2680	mg/kg	1.0			
Aromatic TPH > C8-C10	M	2680	mg/kg	1.0			
Aromatic TPH >C10-C12	W	2680	mg/kg	1.0			
Aromatic TPH >C12-C16	W	2680	mg/kg	1.0			
Aromatic TPH >C16-C21	n .	2680	mg/kg	1.0			
Aromatic TPH >C21-C35	Σ	2680	mg/kg	1.0			
Aromatic TPH >C35-C44	z	2680	mg/kg	1.0			
Total Aromatic Hydrocarbons	z	2680	_	_			
Total Petroleum Hydrocarbons	z	2680	mg/kg	10.0			
Benzene	Σ	2760	µg/kg	1.0			
Toluene	Σ	2760	µg/kg	1.0			
Ethylbenzene	Σ	2760	µg/kg	1.0			
m & p-Xylene	Σ	2760	µg/kg	1.0			
o-Xylene	M	2760	µg/kg	1.0			
Methyl Tert-Butyl Ether	M	2760		1.0			
Naphthalene	M	2800	mg/kg				
Acenaphthylene	z	2800	mg/kg	$\rightarrow$			
Acenaphthene	M	2800	mg/kg	0.10			
Fluorene	Σ	2800	mg/kg	_			
Phenanthrene	Σ	2800	mg/kg	0.10			
Benzo[j]fluoranthene	z	2800	mg/kg				
Anthracene	Σ	2800	mg/kg	0.10			
Fluoranthene	Σ	2800	mg/kg	0.10			
Pyrene	M	2800	mg/kg	0.10			-
Benzo[a]anthracene	M	2800	mg/kg	0.10			
Chrysene	M	2800	mg/kg	0.10			
Benzo[b]fluoranthene	M	2800	mg/kg				
Benzo[k]fluoranthene	M	2800	mg/kg	0.10			
Benzo[a]pyrene	Σ	2800	mg/kg				
Indeno(1,2,3-c,d)Pyrene	M	2800	mg/kg	0.10			
Dibenz(a h)Anthracene	z	2800	mg/kg	0.10			



Client: IGSL		Cher	ntest Jo	Chemtest Job No.:	20-10240	20-10240	20-10240
Quotation No.:		hemte	Chemtest Sample ID.:	ple ID.:	996092	60966	996094
Order No.:		Clier	t Samp	Client Sample Ref.:	13551	13553	130581
	1	Sa	Sample Location:	cation:	BH3	EH8	BH4
			Sample	Sample Type:	SOIL	SOIL	SOIL
			Top Depth (m):	oth (m):	1.00	3.00	1.00
		Bot	tom Dep	Bottom Depth (m):	1.00	3.00	1.00
			Asbest	Asbestos Lab:			
Determinand	Accred.	SOP	SOP Units	LOD			
Benzo[g,h,i]perylene	M	2800	2800 mg/kg	0.10			
Coronene	z	2800	2800 mg/kg	0.10			
Total Of 17 PAH's	z	2800	2800 mg/kg	2.0			
PCB 28	n	2815	mg/kg 0.010	0.010			
PCB 52	ח	2815	mg/kg 0.010	0.010			
PCB 90+101	n l	2815	2815 mg/kg 0.010	0.010			
PCB 118	n	2815	2815 mg/kg 0.010	0.010			
PCB 153	n	2815	mg/kg 0.010	0.010			
PCB 138	n	2815	mg/kg	0.010			
PCB 180	n	2815	mg/kg	0.010			
Total PCBs (7 Congeners)	n	2815	2815 mg/kg	0.10			
Total Phenois	Σ	2920	2920 mg/kg 0.30	0.30			





Chemtest Job No:	20-10240				Langtill	Landfill Waste Acceptance Criteria	e Criteria
cilemest cample 10.	10000					FIIIIIS	
Sample Ref:	131830					Stable, Non-	
Sample ID:						reactive	
Sample Location:	TP1					hazardous	Hazardous
Top Depth(m):	0.50				Inert Waste	waste in non-	Waste
Bottom Depth(m):	0.50				Landfill	hazardous	Landfill
Sampling Date:						Landfill	
Determinand	SOP	Accred.	Units				
Total Organic Carbon	2625	M	%	[A] 1.6	3	2	9
Lass On Ignition	2610	Σ	%	5.5	1	1	10
Total BTEX	2760	M	mg/kg	[A] < 0.010	9		
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	1	1	1
TPH Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	200	,	1
Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	,	1
Hd	2010	M		8.2	1	9<	1
Acid Neutralisation Capacity	2015	z	mol/kg	0.031	-	To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
			mg/I	mg/kg	using B	using BS EN 12457 at L/S 10 I/kg	5 10 l/kg
Arsenic	1450	Ω	< 0.0010	< 0.050	0.5	2	25
Barium	1450	n	0.0093	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	1	5
Chromium	1450	n	< 0.0010	< 0.050	0.5	10	70
Copper	1450	n	0.0011	< 0.050	2	20	100
Mercury	1450	n	< 0.00050	< 0.0050	0.01	0.2	2
Molybdenum	1450	n	0.0033	< 0.050	0.5	10	30
Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	20
Antimony	1450	n	< 0.0010	< 0.010	90.0	0.7	5
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	20	200
Chloride	1220	n	< 1.0	< 10	800	15000	25000
Fluoride	1220	n	0.47	4.7	10	150	200
Sulphate	1220	n	16	160	1000	20000	20000
Total Dissolved Solids	1020	Z	85	840	4000	00009	100000
Phenol Index	1920	n	< 0.030	< 0.30	1		
Dissolved Organic Carbon	1610	n	9.5	98	500	800	1000

y mass of test portion/kg	0.090
oisture (%)	15

# Waste Acceptance Criteria





Chemtest Job No:	20-10240				Landfill	LandfIII Waste Acceptance Criteria	e Criteria
Chemtest Sample ID:	996075					Limits	
Sample Ref:	131831					Stable, Non-	
Sample ID:						reactive	
Sample Location:	TP1					hazardous	Hazardous
Top Depth(m):	1.00				Inert Waste	waste in non-	Waste
Bottom Depth(m):	1.00				Landfill	hazardous	Landfill
Sampling Date:						Landfill	La Colonia Col
Determinand	SOP	Accred.	Units				
Total Organic Carbon	2625	M	%	[A] 0.50	3	5	9
Loss On Ignition	2610	M	%	3.7	1	1	10
Total BTEX	2760	Σ	mg/kg	[A] < 0.010	9	1	ı
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	,		
TPH Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	200	1	1
Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	1	1
Hd	2010	M		8.1	1	9×	1
Acid Neutralisation Capacity	2015	z	mol/kg	0.028	,	To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
			l/gm	mg/kg	a Suisn	using BS EN 1245/ at L/S 10 I/Kg	5 10 I/Kg
Arsenic	1450	n	< 0.0010	< 0.050	0.5	2	25
Barium	1450	n	0.0030	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	1	9
Chromium	1450	n	< 0.0010	< 0.050	0.5	10	70
Copper	1450	n	< 0.0010	< 0.050	2	20	100
Mercury	1450	n	< 0.00050	< 0.0050	0.01	0.2	2
Molybdenum	1450	n	< 0.0010	< 0.050	0.5	10	30
Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	90
Antimony	1450	n	< 0.0010	< 0.010	90.0	0.7	5
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	20	200
Chloride	1220	n	< 1.0	< 10	800	15000	25000
Fluoride	1220	n	0.19	1.9	10	150	200
Sulphate	1220	n	3.2	32	1000	20000	20000
Total Dissolved Solids	1020	z	62	620	4000	00009	100000
Phenol Index	1920	n	< 0.030	< 0.30	1		
Dissolved Organic Carbon	1610	n	5.9	29	200	800	1000

	0000
ry mass or test portion/kg	0.090
loisture (%)	16

# Waste Acceptance Criteria

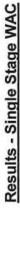




Chemtest Job No:	20-10240				Landfill	Landfill Waste Acceptance Criteria Limits	e Criteria
onemics cample is:						CHILLIAN TO A	
Sample Ref:	131834					Stable, Non-	
Sample ID:						reactive	
Sample Location:	TP2					hazardous	Hazardous
Top Depth(m):	0.50				Inert Waste	waste in non-	Waste
Bottom Depth(m):	0.50				Landfill	hazardous	Landfill
Sampling Date:						Landfill	
Determinand	SOP	Accred.	Units				
Total Organic Carbon	2625	Σ	%	[A] 0.52	3	2	9
Loss On Ignition	2610	Σ	%	3.1	1	1	10
Total BTEX	2760	W	mg/kg	[A] < 0.010	9		
Total PCBs (7 Congeners)	2815	W	mg/kg	< 0.10	1	1	1
TPH Total WAC (Mineral Oil)	2670	W	mg/kg	[A] < 10	200	1	1
Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	1	1
Hd	2010	W		8.5	1	9<	1
Acid Neutralisation Capacity	2015	z	mol/kg	0.12	1	To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
			l/gm	mg/kg	using BS	IS EN 12457 at L/S 10 I/kg	3 10 l/kg
Arsenic	1450	n	< 0.0010	< 0.050	0.5	2	25
Barium	1450	n	0.0065	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	1	5
Chromium	1450	n	< 0.0010	< 0.050	0.5	10	70
Copper	1450	n	0.0014	< 0.050	2	20	100
Mercury	1450	n	< 0.00050	< 0.0050	0.01	0.2	2
Molybdenum	1450	n	0.0076	0.076	0.5	10	30
Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	20
Antimony	1450	n	< 0.0010	< 0.010	90.0	0.7	5
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	20	200
Chloride	1220	n	< 1.0	< 10	800	15000	25000
Fluoride	1220	n	0.27	2.7	10	150	200
Sulphate	1220	n	2.3	23	1000	20000	20000
Total Dissolved Solids	1020	N	65	650	4000	00009	100000
Phenol Index	1920	n	< 0.030	< 0.30	1		
Discolved Organic Carbon	1610	11	19	190	200	800	1000

ry mass of test portion/kg	0.090
thire (%)	12

# Waste Acceptance Criteria





Project: 22455 Avid Development Sandyford (Aecom / Marlet )
Chemtest Job No: 20-10240

Sample Ref:   131838				-	Stable, Non-	
f: 13183 cation: TP3 (m): 0.50 pth(m): 0.50 ate: nd ic Carbon ition (7 Congeners) (7 Congeners) (9 PAH's lisation Capacity lisation Capacity lisation Laboration					Stable, Non-	
cation: TP3 (m): 0.50 pth(m): 0.50 Jate: id ic Carbon lition (7 Congeners) (7 Congeners) (9 PAH's lisation Capacity lisation Capacity						
cation: TP3 (m): 0.50 pth(m): 0.50 Jate: id ic Carbon lition (7 Congeners) (7 Congeners) (9 PAH's lisation Capacity lisation Capacity					reactive	
oco Oco Oco Oco Oco Oco Oco Oco Oco Oco					hazardous	Hazardous
oon geners) fineral Oil) s Capacity				Inert Waste	waste in non-	Waste
arbon ongeners) (Mineral Oil) H's ion Capacity				Landfill	hazardous	Landfill
irbon Orgeners) (Mineral Oil) H's On Capacity					Landfill	
on Capacity	Accred.	Units				
ongeners) (Mineral Oil) H's on Capacity	W	%	[A] 0.98	3	5	9
ongeners) (Mineral Oil) H's on Capacity	W	%	4.4	1	1	10
ongeners) (Mineral Oil) H's on Capacity	W	mg/kg	[A] < 0.010	9		
(Mineral Oil) H's on Capacity	W	mg/kg	< 0.10	- 1	1	1
H's on Capacity	W	mg/kg	[A] < 10	200	1	1
on Capacity	z	mg/kg	< 2.0	100	1	,
on Capacity	W		8.3	•	9<	1
	z	mol/kg	0.083	-	To evaluate	To evaluate
		10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
		mg/l	mg/kg	using B	using BS EN 12457 at L/S 10 I/kg	3 10 l/kg
	n	0.0015	< 0.050	0.5	2	25
Barium 1450	n	0.023	< 0.50	20	100	300
Cadmium 1450	n	< 0.00010	< 0.010	0.04	1	5
Chromium 1450	n	< 0.0010	< 0.050	9.0	10	70
Copper 1450	n	0.0031	< 0.050	2	50	100
Mercury 1450	n	< 0.00050	< 0.0050	0.01	0.2	2
Molybdenum 1450	n	0.0047	< 0.050	0.5	10	30
Nickel 1450	n	0.0018	< 0.050	0.4	10	40
Lead 1450	n	< 0.0010	< 0.010	0.5	10	50
Antimony 1450	ס	0.0015	0.015	90.0	0.7	5
Selenium 1450	n	0.0011	0.011	0.1	0.5	7
Zinc 1450	כ	< 0.0010	< 0.50	4	90	200
Chloride 1220	n	< 1.0	< 10	800	15000	25000
Fluoride 1220	n	0.27	2.7	10	150	500
Sulphate 1220	n	5.7	57	1000	20000	50000
Total Dissolved Solids 1020	z	100	1000	4000	00009	100000
Phenol Index 1920	n	< 0.030	< 0.30	1		
Dissolved Organic Carbon 1610	n	14	140	200	800	1000

lry mass of test portion/kg	0.090
oisture (%)	13

# Waste Acceptance Criteria





To evaluate Hazardous Waste Landfill Limit values for compliance leaching test 50000 1000 300 100 200 500 20 20 Landfill Waste Acceptance Criteria using BS EN 12457 at L/S 10 l/kg waste in non-To evaluate Stable, Nonhazardous hazardous reactive Landfill Limits 15000 20000 100 50 800 150 9< 9 0.7 20 Inert Waste 0.06 100 20 20 0.0 0.5 20.0 0.5 800 500 9 10:1 Eluate [A] < 0.010 < 0.050 < 0.050 < 0.0050 0.052 < 0.050 < 0.010 [A] 0.35 < 0.050 < 0.50 < 0.010 [A] < 10< 0.010 < 0.50 < 0.10 < 2.0 < 0.30 0.18 10:1 Eluate < 0.0010 < 0.0010 < 0.00050 0.0015 0.0052 < 0.0010 < 0.0010 < 0.0010 < 0.0010 < 0.0010 mg/kg mg/kg mg/kg mol/kg < 0.030 < 1.0 0.23 2.2 Accred z Σ 2625 2610 2760 2760 2815 2800 1450 1450 1450 1450 1450 1450 1450 1450 1220 1220 1610 131839 996078 1.00 1.00 Total PCBs (7 Congeners)
TPH Total WAC (Mineral Oil) Acid Neutralisation Capacity Dissolved Organic Carbon Chemtest Sample ID: otal Dissolved Solids otal Organic Carbon otal (Of 17) PAH's Chemtest Job No: Sample Location: Bottom Depth(m): oss On Ignition Eluate Analysis Sampling Date: rop Depth(m): Shenol Index Sample Ref: Determinand Molybdenum Sample ID: otal BTEX Chromium Sadmium Selenium Antimony Sulphate **Jercury** hloride -luoride opper Arsenic Barium ead

Dry mass of test portion/kg	0.090
(%)	8.6

# Waste Acceptance Criteria



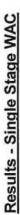


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Project: 22455 Avid Development Sandyford ( Aecom / Marlet )		
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Chemtest Job No:	20-10240				Landfill	Landfill Waste Acceptance Criteria	e Criteria
Chemtest Sample ID:	6/0066					Limits	
Sample Ref:	131842					Stable, Non-	
	101					יפסרואפ	
Sample Location:	47					nazardous	Hazardous
Top Depth(m):	0.50				Inert Waste	waste in non-	Waste
Bottom Depth(m):	0.50				Landfill	hazardous	Landfill
Sampling Date:						Landfill	
Determinand	SOP	Accred.	Units				
Total Organic Carbon	2625	M	%	[A] 0.35	3	2	9
Loss On Ignition	2610	M	%	2.3	1		10
Total BTEX	2760	M	mg/kg	[A] < 0.010	9		
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	1	,	1
TPH Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	200		1
Total (Of 17) PAH's	2800	Z	mg/kg	< 2.0	100		1
Hd	2010	M		8.4		9<	
Acid Neutralisation Capacity	2015	Z	mol/kg	0.18		To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
			l/gm	mg/kg	using B	using BS EN 12457 at L/S 10 l/kg	3 10 I/kg
Arsenic	1450	n	< 0.0010	< 0.050	0.5	2	25
Barium	1450	n	0.0020	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	1	5
Chromium	1450	n	< 0.0010	< 0.050	0.5	10	70
Copper	1450	n	< 0.0010	< 0.050	2	20	100
Mercury	1450	n	< 0.00050	< 0.0050	0.01	0.2	2
Molybdenum	1450	n	0.0074	0.074	0.5	10	30
Nickel	1450	n.	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	20
Antimony	1450	n	< 0.0010	< 0.010	90.0	0.7	2
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	20	200
Chloride	1220	n	1.1	11	800	15000	25000
Fluoride	1220	n	0.24	2.4	10	150	200
Sulphate	1220	n	7.1	71	1000	20000	20000
Total Dissolved Solids	1020	z	22	570	4000	00009	100000
Phenol Index	1920	Þ	< 0.030	< 0.30	-		ı
Dissolved Organic Carbon	1610	=	A A	56	200	000	4000

COLIG IIII CHIII CHI	
Dry mass of test portion/kg	060'0
Moisture (%)	8.2

# Waste Acceptance Criteria





Sample   December   D	Chemtest Job No:	20-10240				Landfill	Landfill Waste Acceptance Criteria	e Criteria
Fig.   131846   Cardions   Card	Chemtest Sample ID:	996080					Limits	
TPS   Carbon   Capton   Capt	Sample Ref:	131846					Stable, Non-	
Post-parish	Sample ID:						reactive	
Ineat Waste   Depth(m);   O.50   Depth(m);   O.50	Sample Location:	TP5					hazardous	Hazardous
Ming Date:	Top Depth(m):	0.50				Inert Waste	waste in non-	Waste
Initial Date:   SOP   Accred.   Units   M	Bottom Depth(m):	0.50				Landfill	hazardous	Landfill
millinand         SOP         Accred.         Units         [A] 0.31         3         5           Origanic Carbon         2656         M         %         1.7         —         —           Origanic Carbon         2610         M         mg/kg         [A] < 0.010         6         —           BTEX         2760         M         mg/kg         [A] < 0.010         6         —         —           PCBs (7 Congeners)         2815         M         mg/kg         [A] < 10         500         —         —           PCB (7 Congeners)         2816         M         mg/kg         [A] < 10         500         —         —           PCB (7 T2) PAH's         2800         N         mg/kg         A.2.0         —	Sampling Date:						Landfill	
Organic Carbon         2625         M         %         [A] 0.31         3         5           Organic Carbon         2610         M         %         1,7          -           On Ignition         2610         M         mg/kg         [A] < 0.01	Determinand	SOP	Accred.	Units		ř.		
Post	Total Organic Carbon	2625	M	%	[A] 0.31	3	5	9
Part	Loss On Ignition	2610	M	%	1.7	,	1	10
PCBS (7 Congeners)         2815         M         mg/kg         < 0.10         1         -           Intal WAC (Mineral Oil)         2670         M         mg/kg         < 0.10	Total BTEX	2760	M	mg/kg	[A] < 0.010	9	1	1
Cotal WAC (Mineral Oil)         2670         M         mg/kg         (A) < 10         500            (Of 17) PAH's         2800         N         mg/kg         <2,0	Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	,	1	
(Of 17) PAH'S         2800         N         mg/kg         < 2.0         10.0         —         >6           Veutralisation Capacity         2010         M         mol/kg         < 2.0         10.5         —         >6           Veutralisation Capacity         2015         N         mol/kg         0.18         —         >6           A Analysis         mol/kg         0.0         0.001         < 0.050         0.5         —         >6           in         mol/kg         U         0.0011         < 0.050         0.5         0.0         100           in         mol/kg         U         0.0011         < 0.050         0.5         1         100           in         mol/kg         U         0.0011         < 0.050         0.5         1         1           in         mol/kg         U         < 0.0010         < 0.050         0.5         1         1           in         mol/kg         U         < 0.0010         < 0.050         0.5         1         1           in         mol/kg         U         < 0.0010         < 0.050         0.5         0         1           in         mol/kg         U         < 0.0010	TPH Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	200	1	1
Veutralisation Capacity         2010         M         mol/kg         10.5          >6           Veutralisation Capacity         2015         N         mol/kg         0.18          To evaluate           e Analysis         mol/kg         0.18          To evaluate           in         1450         U         0.0011         < 0.050         20         1           in/m         1450         U         0.0010         < 0.050         20         10         10           in/m         1450         U         0.00010         < 0.050         20         10         0.0           in/m         1450         U         < 0.0010         < 0.050         2         50         10           in/m         1450         U         < 0.0010         < 0.050         0.0         2         50           In/m         1450         U         < 0.0050         0.050         0.0         0.0         0.0           In/m         1450         U         < 0.0050         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0         0.0 </td <td>Total (Of 17) PAH's</td> <td>2800</td> <td>z</td> <td>mg/kg</td> <td>&lt; 2.0</td> <td>100</td> <td>1</td> <td>-</td>	Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	1	-
Veutralisation Capacity         2015         N         mol/kg         0.18          To evaluate           Fe Analysis         Malysis         Malysis         Malysis         Malysis          To evaluate	Hd	2010	M		10.5	,	9<	
e Analysis         10:1 Eluate         10:1 Eluate         10:1 Eluate           iic         1450         U         0.0011         < 0.050	Acid Neutralisation Capacity	2015	z	mol/kg	0.18	1	To evaluate	To evaluate
iic         1450         U         0.0011         < 0.050         0.5         2           m         1450         U         0.0011         < 0.050	Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	for compliance I	eaching test
lic         1450         U         0.0011         < 0.050         0.5         2           m         1450         U         0.023         < 0.50         20         100           mium         1450         U         < 0.00010         < 0.050         0.5         10           er         1450         U         < 0.00010         < 0.050         2         50         10           der         1450         U         < 0.00059         0.0450         0.5         10         0.2           denum         1450         U         < 0.00059         0.0450         0.5         10           ony         1450         U         < 0.0010         < 0.050         0.4         10           ium         1450         U         < 0.0010         < 0.010         0.05         0.0           ium         1450         U         < 0.0010         < 0.010         0.05         0.0           ium         1450         U         < 0.0010         < 0.010         0.05         0.0         0.0           de         1220         U         < 1.0         < 1.0         0.0         0.0         0.0           de         1220         U				l/gm	mg/kg	using B	S EN 12457 at L/S	3 10 I/kg
mh         1450         U         0.023         < 0.50         20         100           ilum         1450         U         < 0.00010         < 0.010         0.04         1           nilum         1450         U         0.00041         < 0.050         0.5         10           arr         1450         U         0.00069         0.0059         0.01         0.01           Juny         1450         U         0.00069         0.0050         0.01         0.0           Juny         1450         U         0.00069         0.0050         0.0         10           Juny         1450         U         0.00069         0.0050         0.0         10           Juny         1450         U         0.00069         0.0050         0.4         10           Juny         1450         U         0.0010         0.010         0.0         0.0           Juny         1450         U         0.0010         0.010         0.0         0.0           Juny         1450         U         0.0010         0.010         0.0         0.0           Juny         1220         U         0.010         0.0         0.0         0	Arsenic	1450	n	0.0011	< 0.050	0.5	2	25
tium         1450         U         < 0.00010         < 0.010         0.04         1           nium         1450         U         0.0041         < 0.050	Barium	1450	n	0.023	< 0.50	20	100	300
nium         1450         U         0.0041         < 0.050         0.5         10           er         1450         U         < 0.0010	Cadmium	1450	n	< 0.00010	< 0.010	0.04	1	5
er         1450         U         < 0.0010         < 0.050         2         50           July         1450         U         0.00069         0.016         0.01         0.02           Jodenum         1450         U         0.0034         < 0.050	Chromium	1450	n	0.0041	< 0.050	0.5	10	70
July         1450         U         0.00069         0.0069         0.01         0.0059         0.01         0.02           Jodenum         1450         U         0.0034         < 0.050	Copper	1450	n	< 0.0010	< 0.050	2	20	100
Independent         1450         U         0.0034         < 0.050         0.5         10           Independent         1450         U         < 0.0010	Mercury	1450	n	0.00069	0.0069	0.01	0.2	2
I         1450         U         < 0.0010         < 0.050         0.4         10           ony         1450         U         < 0.0010	Molybdenum	1450	n	0.0034	< 0.050	0.5	10	30
ony         1450         U         < 0.0010         < 0.010         0.5         10           lum         1450         U         < 0.010	Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
only         1450         U         < 0.0010         < 0.010         0.06         0.7           ilum         1450         U         0.0010         0.010         0.1         0.5           ide         1220         U         < 1.0	Lead	1450	n	< 0.0010	< 0.010	0.5	10	50
lium         1450         U         0.0010         0.010         0.01         0.01         0.01         0.01         0.01         0.01         4         50           Ide         1220         U         <1.0	Antimony	1450	n	< 0.0010	< 0.010	90:0	0.7	5
ide         1450         U         0.011         < 0.50         4         50           ide         1220         U         < 1.0	Selenium	1450	n	0.0010	0.010	0.1	0.5	7
1220         U         <1.0         <10         800         15000           1220         U         0.14         1.4         10         150           1220         U         310         100         20000           solved Solids         1020         N         400         4000         60000           idex         1920         U         <0.030	Zinc	1450	n	0.011	< 0.50	4	90	200
1220         U         0.14         1.4         10         150           1220         U         310         1000         20000           solved Solids         1020         N         400         4000         60000           idex         1920         U         < 0.30	Chloride	1220	n	< 1.0	< 10	800	15000	25000
solved Solids         1220         U         310         1000         20000           solved Solids         1020         N         400         4000         4000         60000           idex         1920         U         < 0.030         1         -           1 Organic Carbon         1610         U         3.7         < 50         500         800	Fluoride	1220	n	0.14	1.4	10	150	200
1020         N         4000         4000         60000           1920         U         < 0.030	Sulphate	1220	n	310	3100	1000	20000	50000
1920 U <0.030 <0.30 1 - 1610 U 3.7 <50 500 800	Total Dissolved Solids	1020	z	400	4000	4000	00009	100000
1610 U 3,7 <50 500 800	Phenol Index	1920	n	< 0.030	< 0.30	-		
	Dissolved Organic Carbon	1610	ח	3.7	< 50	200	800	1000

Solid Illioninghon	
Ory mass of test portion/kg	060.0
Aoisture (%)	5.9

# Waste Acceptance Criteria





To evaluate Hazardous Waste Limit values for compliance leaching test 50000 Landfill 25000 1000 300 100 200 500 20 40 20 Landfill Waste Acceptance Criteria using BS EN 12457 at L/S 10 l/kg waste in non-To evaluate Stable, Nonhazardous hazardous reactive Landfill 20000 Limits 15000 100 0.7 800 10 0.2 10 150 9 20 9 10 20 Inert Waste 1000 0.06 100 20 20 0.0 0.0 0.5 0.5 800 500 [A] < 0.010 10:1 Eluate < 0.050 < 0.050 < 0.0050 < 0.050 < 0.050 < 0.010 < 0.050 < 0.50 < 0.010 [A] < 10 < 2.0 < 0.010 < 0.010 [A] 0.61 < 0.10 8.0 < 0.50 160 63 10:1 Eluate 0.0010
 0.00050
 0.0041
 0.0010 mg/l0.00100.00610.00010 < 0.0010 < 0.0010 mg/kg 0.0010 Units mg/kg mg/kg mg/kg mol/kg < 0.030 0.26 85 16 6.3 Accred. Σ Σ z Σ SOP 2625 2610 2760 2815 2810 2800 1450 1450 1450 1450 1450 1450 1450 1450 1220 1220 1450 1220 1610 131847 175 120 120 otal PCBs (7 Congeners)
PH Total WAC (Mineral Oil) Acid Neutralisation Capacity Dissolved Organic Carbon Chemtest Sample ID: otal Dissolved Solids otal Organic Carbon Total (Of 17) PAH's Chemtest Job No: Bottom Depth(m): Sample Location: oss On Ignition Eluate Analysis Sampling Date: Top Depth(m): Sample Ref: **Determinand** henol Index **Jolybdenum** Sample ID: Total BTEX Chromium Sadmium elenium untimony nloride ulphate ercury luonde Arsenic opper Barium ead

Dry mass of test portion/kg	0.090
ojetrira (%)	17

# Waste Acceptance Criteria





Limit values for compliance leaching test Landfill Waste Acceptance Criteria using BS EN 12457 at L/S 10 l/kg waste in non-To evaluate Stable, Nonhazardous hazardous reactive Landfill 50 100 0.5 150 >6 10 5 5 10 0.7 Inert Waste 1000 0.06 20 20 0.04 100 0.5 2 0.01 0.5 0.5 8 6 500 10:1 Eluate [A] < 0.010 < 0.050</li>< 0.050</li>< 0.0050</li>< 0.050</li>< 0.050</li>< 0.050</li> [A] < 0.20< 0.050 < 0.50 < 0.010 < < 0.010 [A] < 10 < 2.0 < 0.50 10.8 230 < 50 10:1 Eluate 0.0029 0.0040 < 0.00010 0.0040 < 0.0010 < 0.00050 < 0.0010 < 0.0010 < 0.0010 < 0.0010 mg/kg mg/kg mg/kg mol/kg 0.0031 < 1.0 2 2 Σ Project: 22455 Avid Development Sandyford ( Aecom / Marlet ) 2625 2610 2760 2815 2815 2800 1450 1450 1450 1450 1450 1450 1450 1450 1450 1450 1220 1220 1020 1920 1610 996082 0.50 0.50 'PH Total WAC (Mineral Oil) Acid Neutralisation Capacity Dissolved Organic Carbon otal PCBs (7 Congeners) Chemtest Sample ID: otal Dissolved Solids otal Organic Carbon otal (Of 17) PAH's Chemtest Job No: Bottom Depth(m): Sample Location: oss On Ignition Eluate Analysis Sampling Date: 'op Depth(m): Determinand Phenol Index Sample Ref: Molybdenum Sample ID: otal BTEX Chromium Selenium Cadmium Antimony uoride Sulphate Mercury Chloride Copper Arsenic Barium ead

To evaluate

100

40 20

300 20

Hazardous

Waste Landfill

0.090 0.090 0.090 0.090 0.090 0.090	Solid Illionillation	
7.3 (%)	Dry mass of test portion/kg	060.0
	Noisture (%)	7.3

100000

1000

25000

200

### Waste Acceptance Criteria

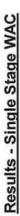




Chemtest Job No:	000000				Landfill	Landfill Waste Acceptance Criteria	e Criteria
Chemtest sample IU:	230083					Limits	
Sample Ref:	136807					Stable, Non-	
Sample ID:						reactive	
Sample Location:	TP7					hazardous	Hazardous
Top Depth(m):	1.00				Inert Waste	waste in non-	Waste
Bottom Depth(m):	1.00				Landfill	hazardous	Landfill
Sampling Date:						Landfill	
Determinand	SOP	Accred.	Units				
Total Organic Carbon	2625	M	%	[A] 0.28	3	2	9
Loss On Ignition	2610	Σ	%	2.5	,	1	10
Total BTEX	2760	M	mg/kg	[A] < 0.010	9	1	ı
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	1	1	1
TPH Total WAC (Mineral Oil)	2670	Σ	mg/kg	[A] < 10	200		1
Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	1	1
Hd	2010	M	1	8.6	1	9<	1
Acid Neutralisation Capacity	2015	z	mol/kg	0.19	1	To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance le	leaching test
			I/Bm	mg/kg	B nsing B	using BS EN 12457 at L/S 10 I/kg	3 10 I/kg
Arsenic	1450	n	< 0.0010	< 0.050	0.5	2	25
Barium	1450	n	0.0072	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	+	2
Chromium	1450	n	< 0.0010	< 0.050	0.5	10	02
Copper	1450	n	< 0.0010	< 0.050	2	20	100
Mercury	1450	n	< 0.00050	< 0.0050	0.01	0.2	2
Molybdenum	1450	n	0.014	0.14	0.5	10	30
Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	20
Antimony	1450	n	< 0.0010	< 0.010	90.0	0.7	5
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	20	200
Chloride	1220	n	< 1.0	< 10	800	15000	25000
Fluoride	1220	n	0.29	2.9	10	150	200
Sulphate	1220	n	2.0	20	1000	20000	20000
Total Dissolved Solids	1020	z	65	650	4000	00009	100000
Phenol Index	1920	n	< 0.030	< 0.30	1		
Dissolved Organic Carbon	1610	n	4.8	< 50	500	800	1000

y mass of test portion/kg	0.090
(%)	44

# Waste Acceptance Criteria





temtest Job No:	20-10240				Landill	Landfill Waste Acceptance Criteria Limits	e Criteria
male Dof	136811					Ctable Men	
mple Net.						reactive	
mple Location:	TP8					hazardous	Hazardous
p Depth(m):	1.00		,		Inert Waste	waste in non-	Waste
ottom Depth(m):	1.00				Landfill	hazardous	Landfill
impling Date:						Landfill	
terminand	SOP	Accred.	Units				
tal Organic Carbon	2625	M	%	[A] 0.35	က	2	9
ss On Ignition	2610	M	%	2.2	,		10
tal BTEX	2760	M	mg/kg	[A] < 0.010	9	1	1
tal PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	-		1
H Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	200		1
ital (Of 17) PAH's	2800	Z	mg/kg	< 2.0	100	1	,
	2010	M		8.6	1	9<	,
id Neutralisation Capacity	2015	z	mol/kg	0.17	1	To evaluate	To evaluate
uate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
	-		l/gm	mg/kg	using B	using BS EN 12457 at L/S 10 l/kg	5 10 l/kg
senic	1450	n	< 0.0010	< 0.050	0.5	2	25
rium	1450	n	0.0014	< 0.50	20	100	300
dmium	1450	n	< 0.00010	< 0.010	0.04	1	5
Iromium	1450	n	< 0.0010	< 0.050	0.5	10	70
pper	1450	n	< 0.0010	< 0.050	2	90	100
ercury	1450	n	< 0.00050	< 0.0050	0.01	0.2	2
olybdenum	1450	n	0.0089	0.089	0.5	10	30
ckel	1450	n	< 0.0010	< 0.050	0.4	10	40
ad	1450	n	< 0.0010	< 0.010	0.5	10	20
timony	1450	n	< 0.0010	< 0.010	90.0	0.7	5
lenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
10	1450	n	< 0.0010	< 0.50	4	90	200
lloride	1220	n	< 1.0	< 10	800	15000	25000
Joride	1220	n	0.19	1.9	10	150	200
Iphate	1220	n	1.4	14	1000	20000	20000
tal Dissolved Solids	1020	Z	49	490	4000	00009	100000
enol Index	1920	n	< 0.030	< 0.30	1	,	
scolved Organic Carbon	1610	-17	5.7	57	500	OUR	1000

Iny mass of test portion/kg	0.090
170/ 07	0

# Waste Acceptance Criteria





To evaluate Hazardous Waste 50000 Limit values for compliance leaching test Landfill 25000 1000 300 200 9 20 LandfIII Waste Acceptance Criteria using BS EN 12457 at L/S 10 l/kg waste in non-To evaluate Stable, Nonhazardous hazardous reactive Landfill Limits 100 800 0.2 150 9 9 10 0.7 20 20 Inert Waste 1000 20 20 0.04 90.0 500 100 0.5 0.01 0.5 0.5 500 0.1 10:1 Eluate [A] < 0.010< 0.050 < 0.050 < 0.050 < 0.0050 < 0.050 < 0.50 < 0.010 [A] < 10 0.15 < 0.050 < 0.010 [A] 0.56 < 0.010 < 0.10 mg/kg 0.011 < 0.50 420 9.9 10:1 Eluate 0.0017 0.0043 < 0.00010 < 0.00010 0.015 < 0.0010 < 0.0010 < 0.0010 < 0.0010 mg/kg mg/kg mg/kg 0.0018 0.0011 < 0.030 mol/kg mg/kg 0.23 42 120 Accred. Σ 2815 2815 2670 2800 1450 1450 1450 1450 2010 1450 1450 1450 1220 1220 1220 1920 1610 996085 136814 0.50 0.50 PH Total WAC (Mineral Oil) Acid Neutralisation Capacity Dissolved Organic Carbon otal PCBs (7 Congeners) otal Dissolved Solids Chemtest Sample ID: otal Organic Carbon otal (Of 17) PAH's Chemtest Job No: Bottom Depth(m): Sample Location: oss On Ignition Eluate Analysis Sampling Date: op Depth(m): eterminand henol Index Sample Ref: olybdenum Sample ID: otal BTEX Chromium adminm ntimony elenium Sulphate uoride Arsenic opper ercury ickel ead inc

Solid Illigillianoil	
y mass of test portion/kg	0.090
oisture (%)	8.5

# Waste Acceptance Criteria



Hazardous

Waste Landfill



Limit values for compliance leaching test Landfill Waste Acceptance Criteria using BS EN 12457 at L/S 10 I/kg waste in non-To evaluate Stable, Nonhazardous hazardous reactive Landfill 15000 20000 100 800 0.2 0.5 150 9 10 5 5 10 0.7 20 20 Inert Waste 1000 0.06 20 20 0.0 500 100 2 2 0.01 0.5 0.5 900 500 10:1 Eluate [A] < 0.010 < 0.050 < 0.050 < 0.050 < 0.0050 < 0.050 < 0.50 < 0.010 0.0710.0500.010 [A] 0.38 [A] < 10 < 0.010 < 0.010 < 2.0 < 0.10 < 0.50 < 0.30 10:1 Eluate < 0.00010 0.0019 < 0.0010 < 0.0010 < 0.0010 < 0.0010 < 0.0010 mol/kg < 0.0010 < 0.0010 mg/kg mg/kg mg/kg mg/kg < 0.030 0.0071 < 1.0 0.19 53 Accred Project: 22455 Avid Development Sandyford ( Aecom / Marlet ) 2815 2815 2670 2800 1450 1450 1450 1450 1450 1450 1450 1450 1450 1220 1220 1610 1920 996086 TP10 1.00 Total PCBs (7 Congeners)
TPH Total WAC (Mineral Oil) Acid Neutralisation Capacity Dissolved Organic Carbon otal Dissolved Solids Chemtest Sample ID: otal Organic Carbon otal (Of 17) PAH's Chemtest Job No: Bottom Depth(m): Sample Location: oss On Ignition Eluate Analysis Sampling Date: op Depth(m): Determinand henol Index Sample Ref: Molybdenum Sample ID: otal BTEX Chromium Cadmium Selenium Antimony Sulphate Copper Mercury hloride noride Arsenic Barium ead

To evaluate

300

100

40 50

20

Dry mass of test portion/kg	0.090
Moisting (%)	40

50000

1000

25000

200

## Waste Acceptance Criteria





Chemtest Job No: Chemtest Sample ID:	20-10240 996087				Landfill	Landfill Waste Acceptance Criteria Limits	e Criteria
	0000						
Sample Ref:	138822					Stable, Non-	
Sample ID:						reactive	
Sample Location:	TP11					hazardous	Hazardous
Top Depth(m):	0.50				Inert Waste	waste in non-	Waste
Bottom Depth(m):	0.50				Landfill	hazardous	Landfill
Sampling Date:						Landfill	
Determinand	SOP	Accred.	Units			(	
Total Organic Carbon	2625	M	%	[A] 0.31	3	5	9
Loss On Ignition	2610	M	%	2.3	1	1	10
Total BTEX	2760	M	mg/kg	[A] < 0.010	9	1	1
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	1	1	,
TPH Total WAC (Mineral Oil)	2670	M	mg/kg	[A] < 10	200	1	1
Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	1	1
Hd	2010	Σ		8.7		9<	1
Acid Neutralisation Capacity	2015	z	mol/kg	0.14	1	To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
			I/6m	mg/kg	B guisn	using BS EN 12457 at L/S 10 I/kg	5 10 I/kg
Arsenic	1450	n	0.0013	< 0.050	0.5	2	25
Barium _	1450	ס	0.0020	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	1	5
Chromium	1450	n	< 0.0010	< 0.050	0.5	-01	70
Copper	1450	n	< 0.0010	< 0.050	2	20	100
Mercury	1450	n	0.00052	0.0052	0.01	0.2	2
Molybdenum	1450	n	0.0072	0.072	0.5	10	30
Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	20
Antimony	1450	ח	0.0021	0.021	90.0	0.7	5
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	20	200
Chloride	1220	n	< 1.0	< 10	800	15000	25000
Fluoride	1220	ח	0.19	1.9	10	150	200
Sulphate	1220	n	8.3	83	1000	20000	20000
Total Dissolved Solids	1020	Z	49	490	4000	00009	100000
Phenol Index	1920	n	< 0.030	< 0.30	1		
Dissolved Organic Carbon	1610	n	7.7	11	200	800	1000

y mass of test portion/kg	0.090
isture (%)	0 1

# Waste Acceptance Criteria



į,

Hazardous

reactive

Waste Landfill

Landfill

1

To evaluate

94

300

100

100

0.2

10 10 0.7 20

50

20

10



Limit values for compliance leaching test Landfill Waste Acceptance Criteria using BS EN 12457 at L/S 10 I/kg waste in non-hazardous To evaluate Stable, Nonhazardous Inert Waste Landfill 100 20 20 0.04 0.0 0.5 0.5 90.0 800 10:1 Eluate [A] < 0.010 < 0.050 < 0.50 < 0.010 < 0.050 < 0.050 0.0050 [A] < 10 < 2.0 < 0.050 < 0.010 < 0.010 [A] 0.34 < 0.50 < 0.10 8.6 0.14 10:1 Eluate < 0.0010 0.0026 < 0.00010 < 0.0010 < 0.0010 < 0.0010 < 0.0010 < 0.0010 < 0.0010 < 0.0010 mg/kg mg/kg mg/kg mg/kg mol/kg 0.014 < 1.0 0.24 z Σ Project: 22455 Avid Development Sandyford ( Aecom / Marlet ) 2760 2815 2670 2800 2010 2015 1450 1450 1450 1450 1450 1450 1450 1450 1450 1450 1220 996088 136827 **TP12** 1.00 otal PCBs (7 Congeners)
PH Total WAC (Mineral Oil) Acid Neutralisation Capacity Chemtest Sample ID: otal Organic Carbon otal (Of 17) PAH's Chemtest Job No: Bottom Depth(m): Sample Location: oss On Ignition Eluate Analysis Sampling Date: op Depth(m): Determinand Sample Ref: Molybdenum Sample ID: otal BTEX Chromium Cadmium Selenium Antimony hloride Mercury noride Arsenic Copper Barium ead

ry mass of test portion/kg	0.090
(%)	10

50000

20000

1000

200 200

15000

150

1000

800

500

< 0.30

< 0.030

1610

Dissolved Organic Carbon

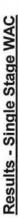
otal Dissolved Solids

Sulphate

nenol Index

54

# Waste Acceptance Criteria





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Project: 22455 Avid Development Sandyford ( Aecom	ı	ľ
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Chemtest Sample ID:	20-10240				Langrill	Landfill Waste Acceptance Criteria	e Criteria
Company of the compan	0000					Fillings	
Sample Ref:	13559					Stable, Non-	
Sample Location	PH4					Posting	The state of the s
Sample Location.						nazardous	Hazardous
Top Depth(m):	1.00				Inert Waste	waste in non-	Waste
Bottom Depth(m):	1.00				Landfill	hazardous	Landfill
Sampling Date:						Landfill	
Determinand	SOP	Accred.	Units				
Total Organic Carbon	2625	M	%	[A] 0.34	3	c)	9
Loss On Ignition	2610	W_	%	2.3	1	1	10
Total BTEX	2760	W	mg/kg	[A] < 0.010	9	:	1
Total PCBs (7 Congeners)	2815	M	mg/kg	< 0.10	1		1
TPH Total WAC (Mineral Oil)	2670	W	mg/kg	[A] < 10	200	1	1
Total (Of 17) PAH's	2800	z	mg/kg	< 2.0	100	1	1
Hd	2010	W		8.5	1	9<	1
Acid Neutralisation Capacity	2015	z	mol/kg	0.17		To evaluate	To evaluate
Eluate Analysis			10:1 Eluate	10:1 Eluate	Limit values	Limit values for compliance leaching test	eaching test
			mg/l	mg/kg	using B	using BS EN 12457 at L/S 10 l/kg	5 10 l/kg
Arsenic	1450	n	< 0.0010	< 0.050	0.5	2	25
Barium	1450	n	0.0031	< 0.50	20	100	300
Cadmium	1450	n	< 0.00010	< 0.010	0.04	+	2
Chromium	1450	n	< 0.0010	< 0.050	0.5	10	70
Copper	1450	n	< 0.0010	< 0.050	2	20	100
Mercury	1450	n	0.00062	0.0062	0.01	0.2	2
Molybdenum	1450	n	0.012	0.12	0.5	10	30
Nickel	1450	n	< 0.0010	< 0.050	0.4	10	40
Lead	1450	n	< 0.0010	< 0.010	0.5	10	20
Antimony	1450	n	< 0.0010	< 0.010	90.0	0.7	2
Selenium	1450	n	< 0.0010	< 0.010	0.1	0.5	7
Zinc	1450	n	< 0.0010	< 0.50	4	- 50	200
Chloride	1220	n	< 1.0	< 10	800	15000	25000
Fluoride	1220	n	0.26	2.6	10	150	200
Sulphate	1220	n	2.1	21	1000	20000	20000
Total Dissolved Solids	1020	z	52	520	4000	00009	100000
Phenol Index	1920	n	< 0.030	< 0.30	1		
Dissolved Organic Carbon	1610	n	5.3	53	200	800	1000

Dry mass of test portion/kg	0.090
(%)	10

# Waste Acceptance Criteria



### **Deviations**

In accordance with UKAS Policy on Deviating Samples TPS 63. Chemtest have a procedure to ensure 'upon receipt of each sample a competent laboratory shall assess whether the sample is suitable with regard to the requested test(s)'. This policy and the respective holding times applied, can be supplied upon request. The reason a sample is declared as deviating is detailed below. Where applicable the analysis remains UKAS/MCERTs accredited but the results may be compromised.

Sample:	Sample Ref:	Sample ID:	Sample Location:	Sampled Date:	Deviation Code(s):	Containers Received:
996074	131830		TP1		Α	Amber Glass 250ml
996074	131830		TP1		А	Plastic Tub 500g
996075	131831		TP1		Α	Amber Glass 250ml
996075	131831		TP1		Α	Plastic Tub 500g
996076	131834		TP2		А	Amber Glass 250ml
996076	131834		TP2		Α	Plastic Tub 500g
996077	131838		TP3		Α	Amber Glass 250ml
996077	131838		TP3		Α	Plastic Tub 500g
996078	131839		TP3		Α	Amber Glass 250ml
996078	131839		TP3		Α	Plastic Tub 500g
996079	131842		TP4		Α	Amber Glass 250ml
996079	131842		TP4		Α	Plastic Tub 500g
996080	131846		TP5		Α	Amber Glass 250ml
996080	131846		TP5		Α	Plastic Tub 500g
996081	131847		TP5		Α	Amber Glass 250ml
996081	131847		TP5		Α	Plastic Tub 500g
996082	131850		TP6		Α	Amber Glass 250ml
996082	131850		TP6		Α	Plastic Tub 500g
996083	136807		TP7		Α	Amber Glass 250ml
996083	136807		TP7		Α	Plastic Tub 500g
996084	136811		TP8		Α	Amber Glass 250ml
996084	136811		TP8		Α	Plastic Tub 500g



### **Deviations**

In accordance with UKAS Policy on Deviating Samples TPS 63. Chemtest have a procedure to ensure 'upon receipt of each sample a competent laboratory shall assess whether the sample is suitable with regard to the requested test(s)'. This policy and the respective holding times applied, can be supplied upon request. The reason a sample is declared as deviating is detailed below. Where applicable the analysis remains UKAS/MCERTs accredited but the results may be compromised.

Sample:	Sample Ref:	Sample ID:	Sample Location:	Sampled Date:	Deviation Code(s):	Containers Received:
996085	136814		TP9		А	Amber Glass 250ml
996085	136814		TP9		А	Plastic Tub 500g
996086	136819		TP10		Α	Amber Glass 250ml
996086	136819		TP10		А	Plastic Tub 500g
996087	138822		TP11		А	Amber Glass 250ml
996087	138822		TP11		А	Plastic Tub 500g
996088	136827		TP12		А	Amber Glass 250ml
996088	136827		TP12		А	Plastic Tub 500g
996089	13559		BH1		Α	Amber Glas 250ml
996089	13559		BH1		А	Plastic Tub 500g
996090	135560		BH1		А	Amber Glass 250ml
996090	135560		BH1		А	Plastic Tub 500g
996091	1		BH2		А	Amber Glas 250ml
996091	1		BH2		А	Plastic Tub 500g
996092	13551		внз		Α	Amber Glas
996092	13551		внз		Α	Plastic Tub 500g
996093	13553		внз		А	Amber Glas 250ml
996093	13553	(	внз		Α	Plastic Tub 500g
996094	130581		BH4		Α	Amber Glas 250ml
996094	130581		BH4	,	Α	Plastic Tub 500g



### **Test Methods**

SOP	Title	Parameters included	Method summary
1010	pH Value of Waters	pH	pH Meter
1020	Electrical Conductivity and Total Dissolved Solids (TDS) in Waters	Electrical Conductivity and Total Dissolved Solids (TDS) in Waters	Conductivity Meter
1220	Anions, Alkalinity & Ammonium in Waters	Fluoride; Chloride; Nitrite; Nitrate; Total; Oxidisable Nitrogen (TON); Sulfate; Phosphate; Alkalinity; Ammonium	Automated colorimetric analysis using 'Aquakem 600' Discrete Analyser.
1450	Metals in Waters by ICP-MS	Metals, including: Antimony; Arsenic; Barium; Beryllium; Boron; Cadmium; Chromium; Cobalt; Copper; Lead; Manganese; Mercury; Molybdenum; Nickel; Selenium; Tin; Vanadium; Zinc	Filtration of samples followed by direct determination by inductively coupled plasma mass spectrometry (ICP-MS).
1610	Total/Dissolved Organic Carbon in Waters	Organic Carbon	TOC Analyser using Catalytic Oxidation
1920	Phenols in Waters by HPLC	Phenolic compounds including: Phenol, Cresols, Xylenols, Trimethylphenols Note: Chlorophenols are excluded.	Determination by High Performance Liquid Chromatography (HPLC) using electrochemica detection.
2010	pH Value of Soils	pH	pH Meter
2015	Acid Neutralisation Capacity	Acid Reserve	Titration
2030	Moisture and Stone Content of Soils(Requirement of MCERTS)	Moisture content	Determination of moisture content of soil as a percentage of its as received mass obtained at <37°C.
2120	Water Soluble Boron, Sulphate, Magnesium & Chromium	Boron; Sulphate; Magnesium; Chromium	Aqueous extraction / ICP-OES
2175	Total Sulphur in Soils	Total Sulphur	Determined by high temperature combustion under oxygen, using an Eltra elemental analyser.
2180	Sulphur (Elemental) in Soils by HPLC	Sulphur	Dichloromethane extraction / HPLC with UV detection
2192	Asbestos	Asbestos	Polarised light microscopy / Gravimetry
2220	Water soluble Chloride in Soils	Chloride	Aqueous extraction and measuremernt by 'Aquakem 600' Discrete Analyser using ferric nitrate / mercuric thiocyanate.
2300	Cyanides & Thiocyanate in Soils	Free (or easy liberatable) Cyanide; total Cyanide; complex Cyanide; Thiocyanate	Allkaline extraction followed by colorimetric determination using Automated Flow Injection Analyser.
2325	Sulphīde în Soils	Sulphide	Steam distillation with sulphuric acid / analysis by 'Aquakem 600' Discrete Analyser, using N,N–dimethyl-p-phenylenediamine.
2430	Total Sulphate in soils	Total Sulphate	Acid digestion followed by determination of sulphate in extract by ICP-OES.
2450	Acid Soluble Metals in Soils	Metals, including: Arsenic; Barium; Beryllium; Cadmium; Chromium; Cobalt; Copper; Lead; Manganese; Mercury; Molybdenum; Nickel; Selenium; Vanadium; Zinc	Acid digestion followed by determination of metals in extract by ICP-MS.
2490	Hexavalent Chromium in Soils	Chromium [VI]	Soil extracts are prepared by extracting dried and ground soil samples into boiling water. Chromium [VI] is determined by 'Aquakem 600 Discrete Analyser using 1,5-diphenylcarbazide
2610	Loss on Ignition	loss on ignition (LOI)	Determination of the proportion by mass that is lost from a soil by ignition at 550°C.
2625	Total Organic Carbon in Soils	Total organic Carbon (TOC)	Determined by high temperature combustion under oxygen, using an Eltra elemental analyser.
2670	Total Petroleum Hydrocarbons (TPH) in Soils by GC-FID	TPH (C6–C40); optional carbon banding, e.g. 3-band – GRO, DRO & LRO*TPH C8–C40	Dichloromethane extraction / GC-FID



### **Test Methods**

SOP	Title	Parameters included	Method summary
2680	TPH A/A Split	Aliphatics: >C5-C6, >C6-C8,>C8-C10, >C10-C12, >C12-C16, >C16-C21, >C21- C35, >C35- C44Aromatics: >C5-C7, >C7-C8, >C8-C10, >C10-C12, >C12-C16, >C16-C21, >C21-C35, >C35-C44	Dichloromethane extraction / GCxGC FID detection
2760	Volatile Organic Compounds (VOCs) in Soils by Headspace GC-MS	Volatile organic compounds, including BTEX and halogenated Aliphatic/Aromatics.(cf. USEPA Method 8260)*please refer to UKAS schedule	Automated headspace gas chromatographic (GC) analysis of a soil sample, as received, with mass spectrometric (MS) detection of volatile organic compounds.
2800	Speciated Polynuclear Aromatic Hydrocarbons (PAH) in Soil by GC-MS	Acenaphthene*; Acenaphthylene; Anthracene*; Benzo[a]Anthracene*; Benzo[a]Pyrene*; Benzo[b]Fluoranthene*; Benzo[ghi]Perylene*; Benzo[k]Fluoranthene; Chrysene*; Dibenz[ah]Anthracene; Fluoranthene*; Fluorene*; Indeno[123cd]Pyrene*; Naphthalene*; Phenanthrene*; Pyrene*	Dichloromethane extraction / GC-MS
2815	Polychlorinated Biphenyls (PCB) ICES7Congeners in Soils by GC-MS	ICES7 PCB congeners	Acetone/Hexane extraction / GC-MS
2920	Phenols in Soils by HPLC	Phenolic compounds including Resorcinol, Phenol, Methylphenols, Dimethylphenols, 1- Naphthol and TrimethylphenolsNote: chlorophenols are excluded.	60:40 methanol/water mixture extraction, followed by HPLC determination using electrochemical detection.
640	Characterisation of Waste (Leaching C10)	Waste material including soil, sludges and granular waste	ComplianceTest for Leaching of Granular Waste Material and Sludge



#### Report Information

#### Key

- U UKAS accredited
- M MCERTS and UKAS accredited
- N Unaccredited
- S This analysis has been subcontracted to a UKAS accredited laboratory that is accredited for this analysis
- SN This analysis has been subcontracted to a UKAS accredited laboratory that is not accredited for this analysis
- T This analysis has been subcontracted to an unaccredited laboratory
- I/S Insufficient Sample
- U/S Unsuitable Sample
- N/E not evaluated
- < "less than"
- > "greater than"

Comments or interpretations are beyond the scope of UKAS accreditation

The results relate only to the items tested

Uncertainty of measurement for the determinands tested are available upon request

None of the results in this report have been recovery corrected

All results are expressed on a dry weight basis

The following tests were analysed on samples as received and the results subsequently corrected to a dry weight basis TPH, BTEX, VOCs, SVOCs, PCBs, Phenols

For all other tests the samples were dried at < 37°C prior to analysis

All Asbestos testing is performed at the indicated laboratory

Issue numbers are sequential starting with 1 all subsequent reports are incremented by 1

#### Sample Deviation Codes

- A Date of sampling not supplied
- B Sample age exceeds stability time (sampling to extraction)
- C Sample not received in appropriate containers
- D Broken Container
- E Insufficient Sample (Applies to LOI in Trommel Fines Only)

#### Sample Retention and Disposal

All soil samples will be retained for a period of 45 days from the date of receipt

All water samples will be retained for 14 days from the date of receipt

Charges may apply to extended sample storage

If you require extended retention of samples, please email your requirements to: <u>customerservices@chemtest.com</u>

### Appendix VI Test Data

c. Water Levels and Gas Concentrations

			Gas & Gro	oundwater	Gas & Groundwater Monitoring		
							(
Site Location	Site Location Carmanhall road	d, Sandyford.					了到
Project No. 22455	22455						(IGST/
Client	Client Marlet					-	
Date	Date 20th March 2020						
	ВНЗ	RC2	BHI	RC4	,		
WATER LEVEL (m bgl)	2.5	2.9	2.2	2.4			1
GAS FLOW	n/a	n/a	n/a	n/a			
СН4(%)	0.0	0.0	0.0	0.0			
LEL(%)	0.0	0.0	0.0	0.0			
CO2(%)	0.1	0.0	0.2	0.0			
02(%)	20.7	19.9	19.6	20.6			
BAROMETRIC PRESURE (mb)	1014	1014	1014	1014			
WEATHER	Sunny	Sunny	Sunny	Sunny			
COMMENTS					3		

			000 00 00	Juliumator	das a diodinament monitoring	
Site Location	Site Location Carmanhall road,	d, Sandyford.				
Project No. 22455	22455					
Client	Client Marlet					
Date	Date 15th May 2020					
	BH3	RC2	BH1	RC4		
WATER LEVEL (m bgl)	2.2	2.6	1.9	2.05		
GAS FLOW	n/a	1⁄2 a	n/a	n/a		
CH4(%)	0.0	0.0	0.0	0.0		
EL(%)	0.0	0.0	0.0	0.0		And the second s
CO2(%)	0.1	0.0	0.1	0.0		
02(%)	20.5	19.7	19.9	20.1		
BAROMETRIC PRESURE (mb)	1006	1006	1006	1006		
WEATHER	Sunny	Sunny	Sunny	Sunny		
			P			and the second
COMMENTS	***************************************					

					0
Site Location	Site Location Carmanhall road,	, Sandyford.			
Project No. 22455	22455				
Client Marlet	Mariet				
Date	16-Jun-20				
Section Displayers and the con-	BH3	RC2	1H8	PC4	
WATER LEVEL (m bgf)	2.1	2.5	1.63	1.83	
GAS FLOW	0.0l/hr	Ol/hr	0l/hr	OV/hr	111111
CH4(%)	0.0	0.0	0.0	0.0	
LEL(%)	0.0	0.0	0.0	0.0	
CO2(%)	0.0	0.0	0.1	0.0	
05(%)	20.7	19.9	20.4	20.6	
BAROMETRIC PRESURE (mb)	1001	1001	1001	1001	
WEATHER	Raining	Raining	Raining	Raining	
COMMENTS					

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Residental Development at Sandyford Avid Site

OFOR

Marlet Property Group

Trial Pil Schedul

	tan'i dag Bart Aust' annongga kisisi sa bahan dar 'kadanodka du seksya pada'ya ab Azbar

CBR Schedule
Hef Position A Pos
CSR-01 71929852 729

Sandyford Business Centre

A B A

12	18 02 2020	Issued for Texter
~	DATE	DESCRIPTION

							60001	REV: POI
STATUS	D2 - Suitable for Tender	UMBER			orks	BER	AVID-ACM-00-XX-DR-S-060001	00
SUITABILITY STATUS	D2 - Suitab	PROJECT NUMBER	PR-461030	SHEET TITLE	Site Investigation Scope of Works	SHEET NUMBER	AVID-ACM-	SCALE: 1:500

	-
Site Investigation Scope of Works	SHEET NUMBER
Step	SKE

5-060001	REY
OD-XX-DR-	00
N	1.50
ID-AC	ALE
	DR-S-060

E. Greenfield Runoff Calculation for proposed site

### Print

### Close Report



Growth curve factor 100 years:

Growth curve factor 200 years:

### Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool Site Details Calculated by: Laura Ruiz Latitude: Site name: Avid Site Longitude: Site location: This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria Reference: 3104524184 in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS Date: May 31 2022 12:30 (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites. Runoff estimation approach Site characteristics Notes Total site area (ha): 0.6 (1) Is  $Q_{BAR} < 2.0 \text{ l/s/ha}$ ? Methodology Q<sub>BAR</sub> estimation method: Calculate from SPR and SAAR When  $Q_{BAR}$  is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha. SPR estimation method: Calculate from SOIL type Edited Default Soil characteristics SOIL type: (2) Are flow rates < 5.0 l/s? 0 3 **HOST class:** N/A N/A Where flow rates are less than 5.0 l/s consent for discharge is SPR/SPRHOST: 0.00 0.37 usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set Default Edited Hydrological characteristics where the blockage risk is addressed by using appropriate SAAR (mm): drainage elements. 0 930 Hydrological region: 1 1 (3) Is SPR/SPRHOST  $\leq 0.3$ ? Growth curve factor 1 year: 0.85 Growth curve factor 30 years: Where groundwater levels are low enough the use of 1.95 soakaways to avoid discharge offsite would normally be

Greenfield runoff rates	Default	Edited
Q <sub>BAR</sub> (I/s):	0	2.4
1 in 1 year (l/s):		2.04
1 in 30 years (l/s):		4.69
1 in 100 year (l/s):		5.96
1 in 200 years (l/s):		6.83

preferred for disposal of surface water runoff.

2.48

2.84

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at www.uksuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

### F. Volume Storage Calculations



Waterman Moylan Consulting

File: Tank Design\_v3.pfd Network: Storm Network

Laura Ruiz 14/07/2022 Page 1

21-118 Avid Site

### **Design Settings**

Rainfall Methodology FSR Return Period (years) 5 Additional Flow (%) 0

FSR Region England and Wales

M5-60 (mm) 17.800 Ratio-R 0.275

CV 0.750

Time of Entry (mins) 4.00

Maximum Time of Concentration (mins) 30.00 Maximum Rainfall (mm/hr) 50.0 Minimum Velocity (m/s) 1.00 Connection Type **Level Soffits** Minimum Backdrop Height (m) 0.000 Preferred Cover Depth (m) 1.200 Include Intermediate Ground ✓ Enforce best practice design rules ✓

#### **Nodes**

Name		Diameter (mm)			Depth (m)
Tank	84.300	1200	35.463	61.845	3.080



### Waterman Moylan Consulting

File: Tank Design\_v3.pfd Network: Storm Network Laura Ruiz 14/07/2022 Page 2 21-118 Avid Site

Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.99%

**Node Event** US Peak Level Depth Inflow Node Flood Status Node (mins) (m) (I/s) Vol (m³) (m³) (m) 2160 minute winter Tank 1920 82.819 1.599 12.1 423.7460 0.0000 OK

Link Event US Link Outflow Discharge (Upstream Depth) Node (I/s) Vol (m³) 2160 minute winter Tank Hydro-Brake® 2.2 241.7

G.	<b>DLRCC</b>	<b>Email</b>	Confirmation for	or Omis	sion of I	Urban	Creep Factor	
----	--------------	--------------	------------------	---------	-----------	-------	--------------	--

#### Laura Ruiz Garrido

From: Cunniffe John <jcunniffe@DLRCOCO.IE>

**Sent:** Friday 24 June 2022 10:31 **To:** Laura Ruiz Garrido

**Cc:** Ian Worrell; Codd Johanne **Subject:** RE: 21-118 AVID SIte.

Hi Laura,

Johanne is actually looking after this one, but to answer the question, yes for this specific site the urban creep factor can be omitted.

The WeTransfer file you sent on previously seems to have corrupted during the download on our end, could you send it again please?

Regards,

John

From: Laura Ruiz Garrido < L. Ruiz@waterman-moylan.ie>

**Sent:** Tuesday 21 June 2022 10:33

To: Cunniffe John < jcunniffe@DLRCOCO.IE>

Cc: Ian Worrell <i.worrell@waterman-moylan.ie>; Codd Johanne <jcodd@DLRCOCO.IE>

Subject: RE: 21-118 AVID SIte.

**CAUTION:** This email originated from outside Dún Laoghaire-Rathdown County Council. Do not click links or open attachments unless you recognise the sender and know the content is safe.

Hi John,

Following my previous email for a drainage design in AVID Site. I wonder if you could confirm that an urban creep factor can be omitted from this specific site. The development is composed of apartment blocks that will be managed by a private management company and there will not be an opportunity for the residents to add hardstanding areas to the development.

Regards,

Laura Ruiz Garrido Project Engineer Waterman Moylan

Block S, EastPoint Business Park, Alfie Byrne Road, Dublin D03 H3F4 t + 353 1 664 8900

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From: Laura Ruiz Garrido <L.Ruiz@waterman-moylan.ie>

**Sent:** Thursday 16 June 2022 16:45

To: Codd Johanne < jcodd@DLRCOCO.IE >

Cc: Cunniffe John < jcunniffe@DLRCOCO.IE >; Ian Worrell < j.worrell@waterman-moylan.ie >

Subject: 21-118 AVID SIte.

Dear Johanne,

I hope you are keeping well.

Please find a link below a response report to the items raised by the DLRCC Drainage Department on the AVID SHD project, Carrickmines. The Planning reference number is Reg. Ref. ABP-312265-21.

#### https://we.tl/t-S6qd7FFwaR

I trust the attached documentation and drawings in the link are satisfactory. Should you have any further questions, please do let me know.

Regards,

Laura Ruiz Garrido Project Engineer Waterman Moylan

Block S, EastPoint Business Park,
Alfie Byrne Road, Dublin D03 H3F4
t + 353 1 664 8900
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